

VILLAGE OF DOBBS FERRY BOARD OF TRUSTEES AGENDA

MEETING DATE: AUGUST 11, 2020

AGENDA ITEM SECTION: PUBLIC HEARING

AGENDA ITEM NO.: 1

AGENDA ITEM: CONTINUATION OF PUBLIC HEARING TO CONSIDER THE APPLICATION OF 115 BROADWAY/ST. CABRINI TO ADD A NEW PARKING LOT ON THEIR PROPERTY

ITEM BACKUP DOCUMENTATION:

- 1. LETTER DATED AUGUST 3, 2020 FROM MR. RALPH PERAGINE, P.E. TO MAYOR VINCENT ROSSILLO AND THE BOARD OF TRUSTEES
- 2. 115 BROADWAY PLANS
- 3. 115 BROADWAY STORMWATER MANAGEMENT REPORT





August 3, 2020

Mayor Vincent Rossillo and Members of the Village Board of Trustees Village of Dobbs Ferry 112 Main Street Dobbs Ferry, NY 10522

RE: Cabrini of Westchester – Application for Site Plan Approval – Parking Lot (25 Spaces) 115 Broadway, Dobbs Ferry, New York

Mayor Vincent Rossillo and Members of the Village Board of Trustees:

We are pleased to submit ten (10) copies of the attached information in support Cabrini of Westchester (the "Applicant") application for Site Plan Approval. The Drawings and Stormwater Management Report have been revised per the Board of Trustees Special Meeting that was held on 7/27/2020.

A. Site Plan Approval Drawings

Drawings p	repared by Provident Design Engineer	ing, PLLC			
Dwg. No.	Title	Sheet	Rev#	Date	
C-10	Overall Site Plan	1	4	8/3/2020	
C-101	Site Plan (North Lot)	2	4	8/3/2020	
C-102	Site Plan (South Lot)	3	1	8/3/2020	
C-201	Grading & Drainage Plan	4	3	8/3/2020	
C-301	Erosion & Sediment Control Plan	5	4	8/3/2020	
C-401	Details	6	3	8/3/2020	
C-402	Details	7	3	8/3/2020	
C-403	Infiltration Bed Details	8	3	8/3/2020	
LP-101	Lighting Plan	9	2	8/3/2020	
Drawings prepared by IQ Landscape Architects, P.C.					
L1	Landscape Plan and Details 1 3 8/3/				

B. Stormwater Management Report dated August 3, 2020.

Please let us know if you need any further information.

Village of Dobbs Ferry Board of Trustees Page 2 August 3, 2020

Very truly yours,

Provident Design Engineering, PLLC

Ralph P. Peragine, P.E. Senior Project Manager

Encs.

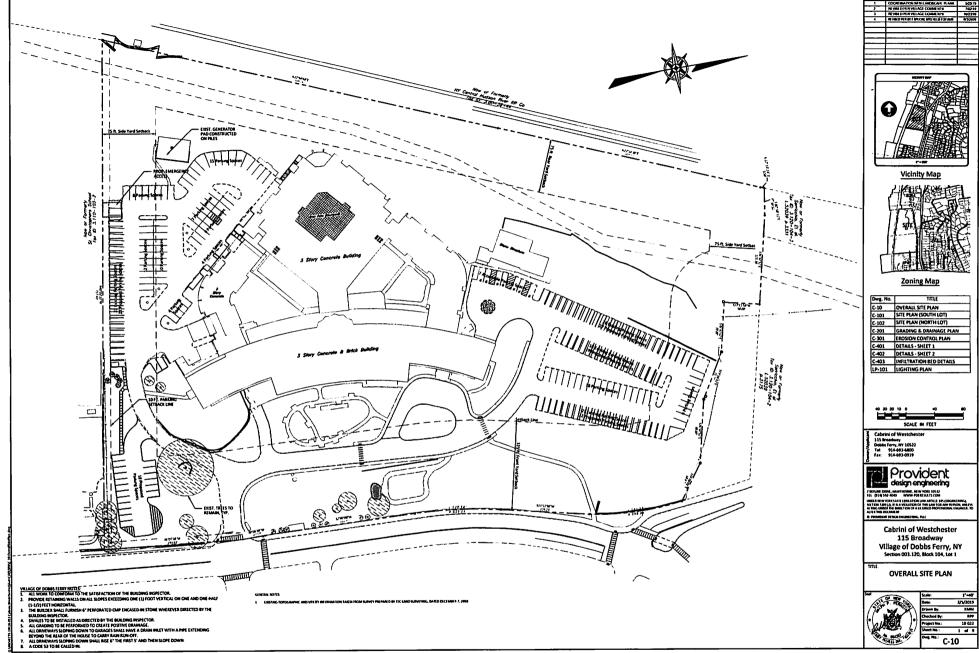
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P. Krauskasky - CEO/President Cabrini of Westchester

T. Palmer – Cuddy and Feder

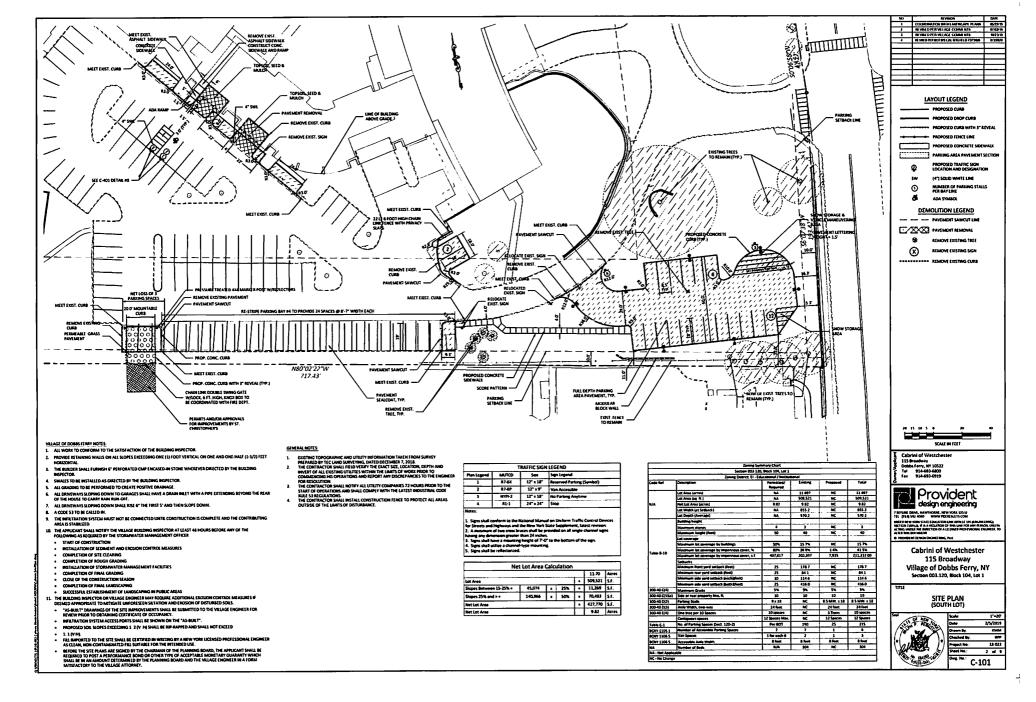
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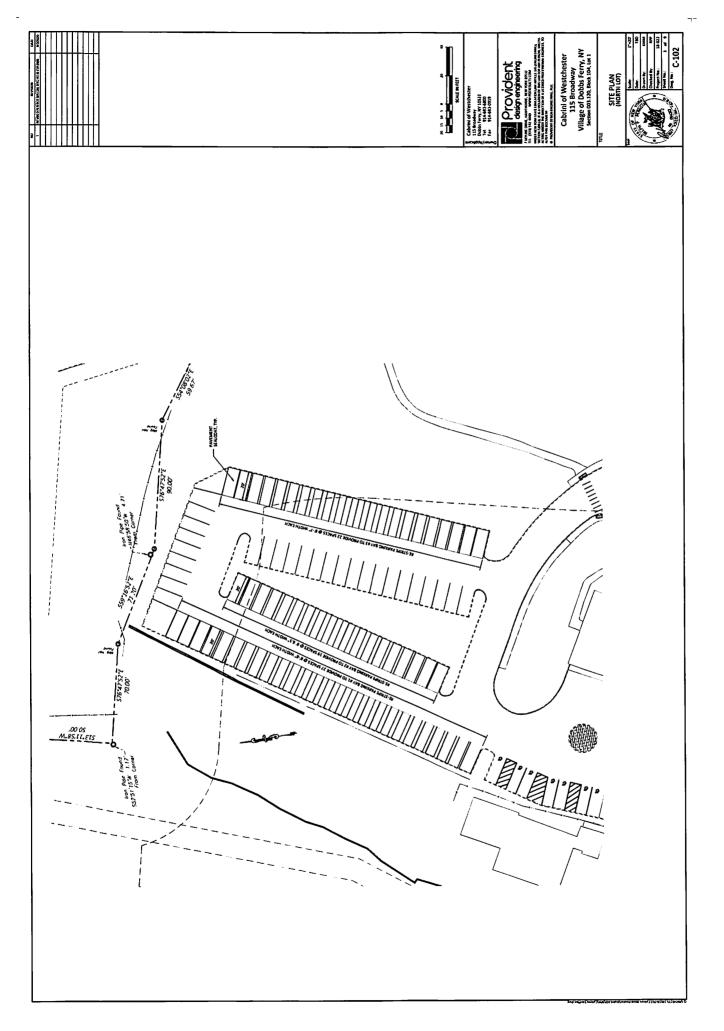


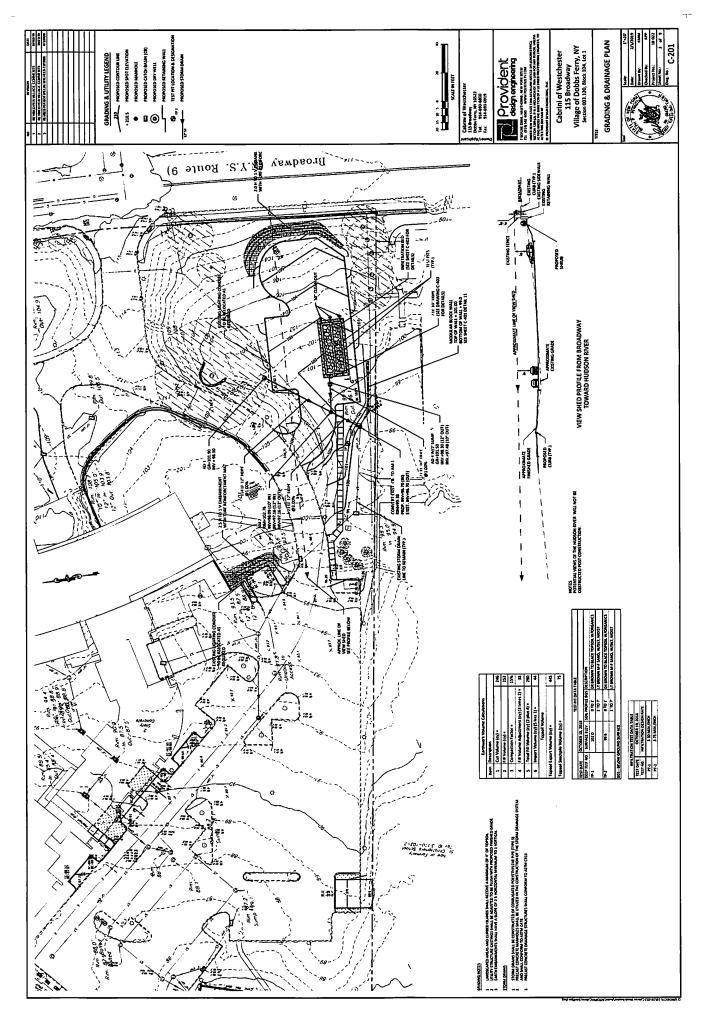


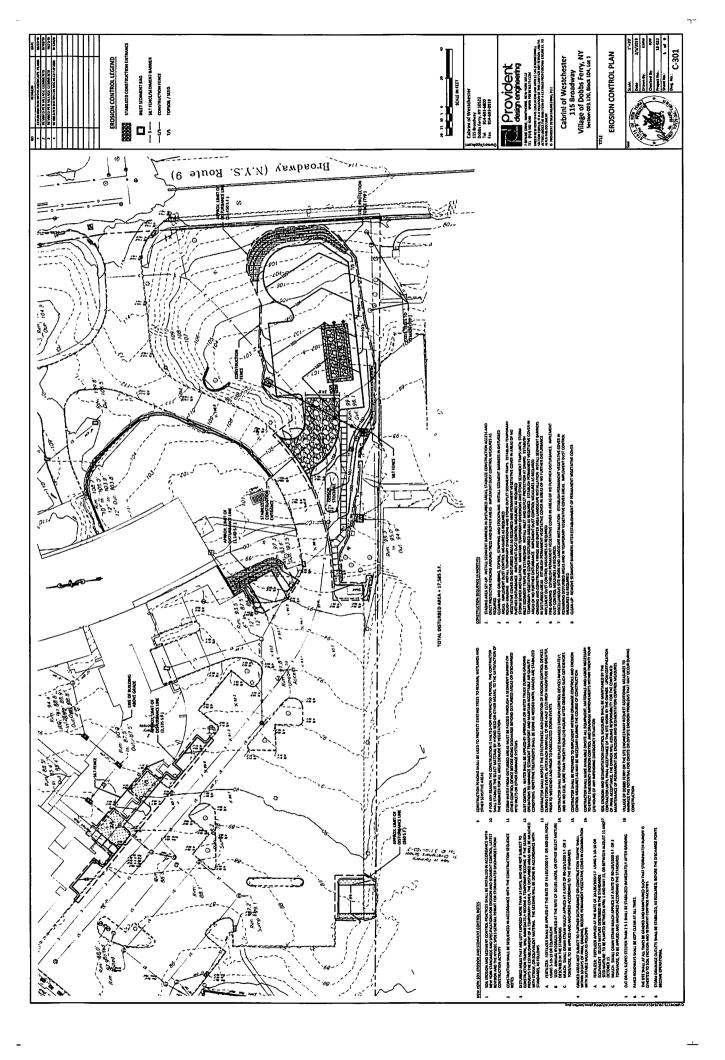
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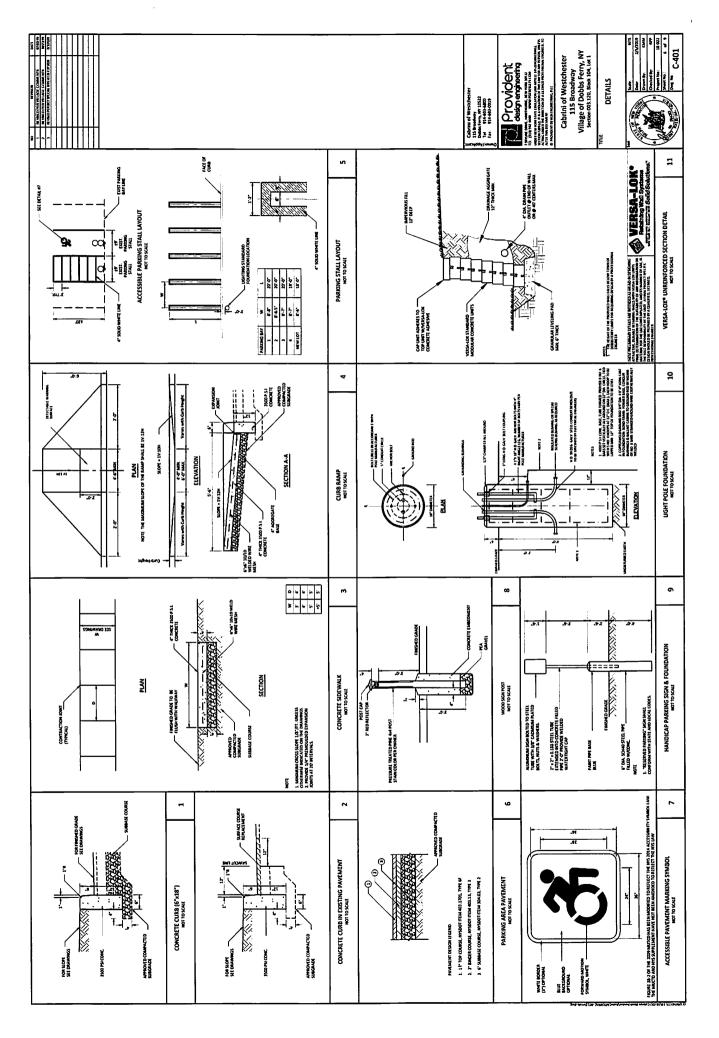


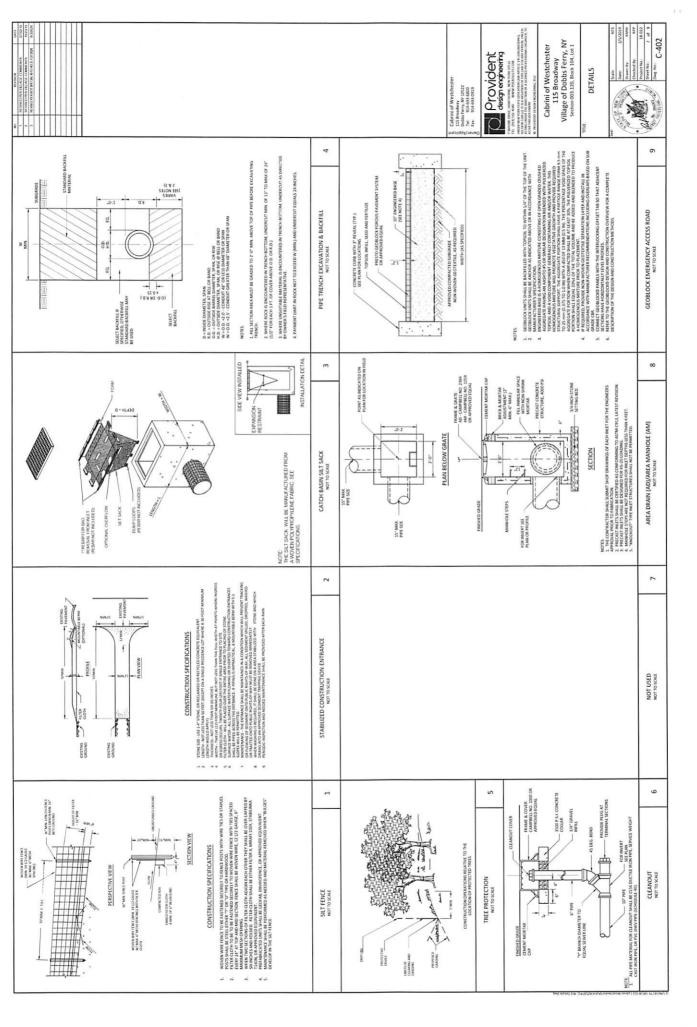
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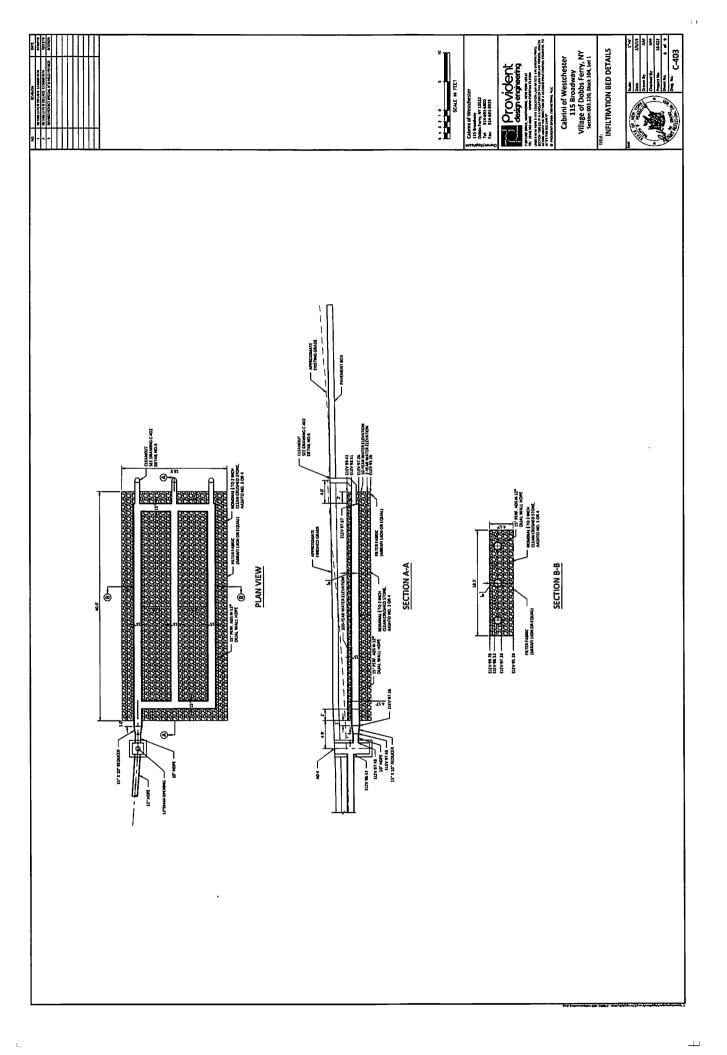


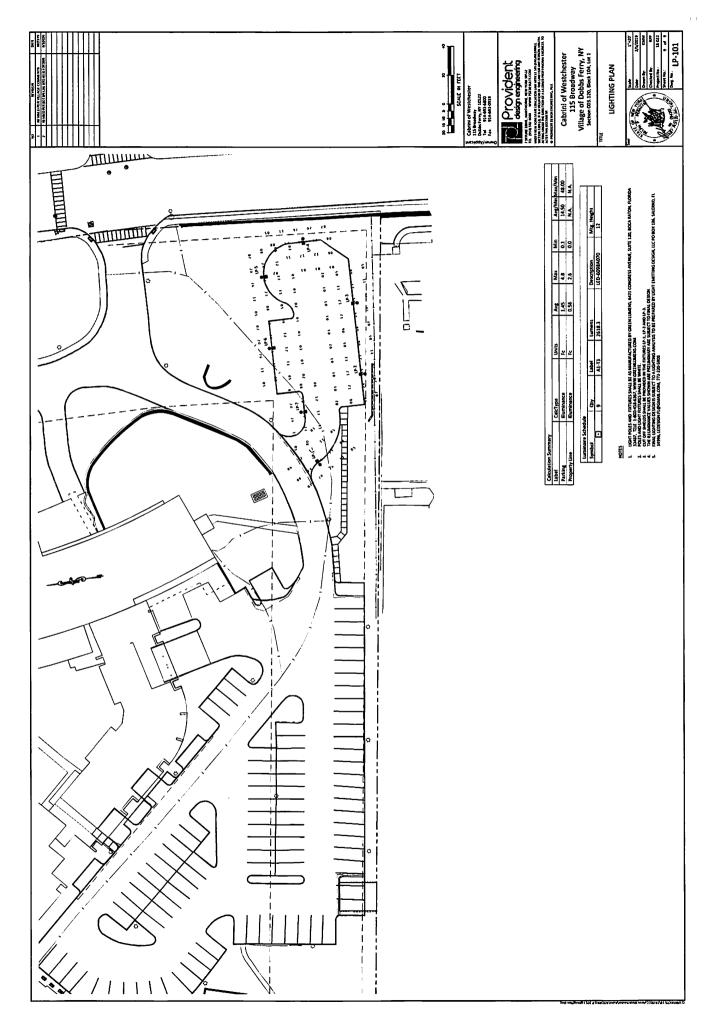


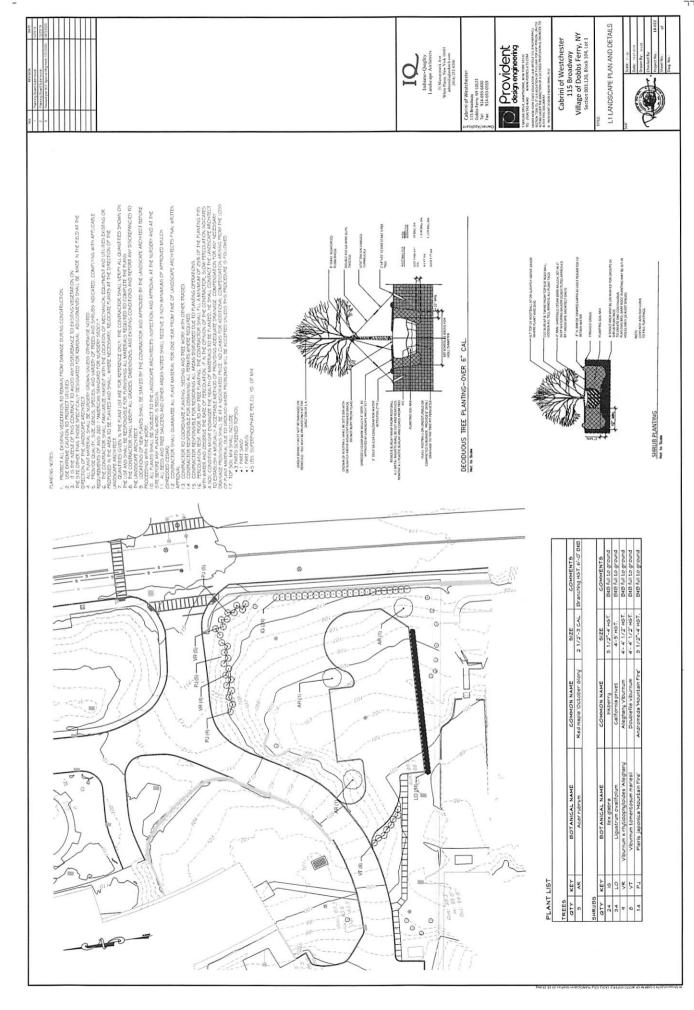
















STORMWATER MANAGEMENT REPORT

CABRINI OF WESTCHESTER PARKING AREA ADDITION 115 BROADWAY VILLAGE OF DOBBS FERRY, NEW YORK

Applicant/Owner

Cabrini of Westchester Parking Area Addition 115 Broadway Village of Dobbs Ferry, New York Tel: (914) 693-6800

Site Engineer

Provident Design Engineering, PLLC

7 Skyline Drive Hawthorne, New York 10532 Tel: (914) 592-4040

Project No.: 18/22

August 3, 2020

Revision History				
Rev. No.	Date	Description		
1	10/23/19	Revised per Village comments		
2	8/3/2020	Revised per BOT special meeting held on 7/27/2020		

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Reference Drawings

Dwg. No.	Title
C-10	Overall Site Plan
C-101	Site Plan
C-201	Grading & Drainage Plan
C-301	Erosion Control Plan
C-401	Details - Sheet 1
C-402	Details - Sheet 2
C-403	Infiltration Bed Details

Section I

Project Information

1.1 Project Description

The purpose of this report is to present the Stormwater Management Report (SWR) for the for the Application for site plan approval to construct a new parking area to accommodate a total of 25 parking spaces which includes eighteen (18) parking spaces in the new parking area to be constructed in the southeasterly corner of the property; two (2) new parking spaces to be constructed adjacent to the existing dumpster pad; and five (5) parking spaces gained by re-striping of four of the existing parking bays to a minimum stall width of 8'-6".

This SWR presents the methodology and design for controlling stormwater runoff from the Project in accordance with the applicable provisions of Chapter 262 Stormwater Management and Erosion and Sediment Control of the Village Code.

1.2 Soil Characteristics

A review of the USDA Web Soil Survey indicates that there are three (3) soil types present on the site (Appendix A). Table No. 1 below summarizes the characteristics of these soil types.

	Table No. 1						
	Soil Characteristics						
Map Unit	Area	Soil Names	Depth to	Depth to	Hydrologic	Erosion	
	(acres)		Water Table	Restrictive	Group	Hazard	
			(ft)	feature			
KnB	2.67	Knickerbocker fine sandy	>80 inches	>80 inches	A		
		loam, 2 to 8 percent slopes					
RhE	2.93	Riverhead loam, 25 to 50	>80 inches	>80 inches	A		
		percent slopes					
Ub	6.09	Udorthents, smoothed	18 to 48	40 to 60	В	Variable	
			inches	inches			

Source: Soil Survey of Westchester and Putnam Counties, New York Soil Conservation Service.
Natural Resource Conservation Center Web Soil Survey

USDA Web Soil Survey (https://websoilsurvey.nrcs.usda.gov/app/WebSoilSurvey.aspx)

Section 2

Storm Water Management

2.1 <u>Methodology</u>

The measures in this SWR Report have been designed to assure that post-development peak runoff rates will be equal to or less than pre-development peak runoff rates for the 2, 10 and 100-year storm events. These measures have been designed in accordance with the following publications:

- "Urban Hydrology for Small Watersheds" (Technical Release No. 55), published by the United States Department of Agriculture, Natural Resources Conservation Service (NRCS) (formerly Soil Conservation Service, SCS), dated June 1986.
- <u>New York State Storm Water Management Design Manual</u> (DEC Design Manual), January 2015.

The 24-hour rainfall data value used in the hydrologic analysis and computations is based on the updated isohyetal maps from the Northeast Regional Climate Center (NRCC). Current 24-hour NRCC rainfall precipitation and distribution data were used to compute runoff hydrographs for the 2, 10 and 100-year storm events. The pre and post development runoff rates for the specified storm events were calculated using HydroCAD® Version 10.0 computer software program. HydroCAD® incorporates the methodology used in NRCS TR-20 and TR-55 to compute and route flood hydrographs.

2.2 <u>Subsurface Investigations</u>

Test Pit Excavations

Two (2) test pits were excavated on October 18, 2018 and witnessed by PDE personnel. The test pit locations are shown on Drawing C-201, "Grading and Utility Plan" prepared by PDE. PDE personnel measured the depths of the contrasting soil layers, performed visual inspections of the excavated material at each layer encountered to determine generalized soil classifications, and logged the measurements and observations.

As shown in the photos and on the test pit log sheets provided in Appendix B, bedrock was not encountered at TP-1 or TP-2. Observations revealed a 12-inch-thick layer of topsoil on top of layers of fine to medium brown sands. The test pits were excavated to a depth of 84 inches below existing grade without encountering ground water.

Infiltration Testing

Based on the investigation results discussed above, two (2) soil infiltration tests were set up on October 18, 2018. A 6" PVC casing was placed adjacent to each test pit as shown on PDE Drawing C-201, with the bottom of the casing set within the existing sand layer at a depth of about 6-feet below existing grade. The casing was filled with 24 inches of water, capped and allowed to pre-soak overnight. PDE personnel returned to the residence on October 19, 2018 and found no water in the casing, thereby allowing the infiltration testing to proceed.

The casing was refilled with 24 inches of water and an initial reading was taken. A "final" reading of the water level was taken after a duration of 1 hour. This procedure was repeated two (2) additional times for a total of three (3) observations at each test pit to obtain the infiltration rate. The data sheet of test results provided in Appendix B shows that the existing subsoils possess a consistent infiltration rate of 18 inches per hour (in/hr.) for TP-1 and 16 in/hr. for TP-2 which are much greater than the minimum rate of 0.5 in/hr. required by the standards in the DEC Design Manual for infiltration SMPs.

2.3 Pre-Development Conditions

Under pre-development conditions, one drainage area (EX-DA-1) was identified on the site. The pre-development drainage areas are shown on Figure #2, Pre-Development Drainage Area Map in Appendix A. The drainage area totals 0.58-acres.

One Design Point was identified for the existing drainage area. The Design Point represent the location where the majority of runoff from an area exits the site. The same design points are identified in post-development conditions so that a comparison can be made between the pre and post development conditions. The area drains to an existing inlet connected to the site's storm drain system.

2.4 Post Development Conditions

Under post development conditions the same design point was identified, however the area was divided into four separate drainage areas. Drainage areas PR-DA-1, and PR-DA-4 will direct discharge in to the storm drain system without being detained. The runoff from PR-DA-2 will be collected by the proposed storm drain system and directed to the proposed stormwater management practice (SMP). The runoff from Drainage area PR-DA-3 will discharge toward the southern property line, however this runoff from this area will not negatively impact the adjacent property. The post development drainage areas are shown on Figure #3, Post Development Drainage Area Map in Appendix A.

In order to assure that post-development peak runoff rates will be equal to or less than predevelopment peak runoff rates, a SMP is required. Based on the results of the subsurface investigation summarized in Section 2.2 above, it is the professional opinion of PDE that a subsurface infiltration/recharge SMP can be provided to attenuate post-construction runoff associated with the construction of the new parking area.

Runoff from the new parking lot in drainage area PR-DA-2 will be collected by the proposed storm drain system and directed to a subsurface gravel bed with 15-inch perforated pipes for infiltration. Table 2, SMP Summary Table, indicates the inflow, outflow, storage volume, water surface elevation, and freeboard of the SMP for the 2, 10 and 100-year design storms.

Table No. 2 – Stormwater Management Summary Table					
Design Year	Peak Inflow (cfs)	Peak Outflow (cfs)	Volume (ft³)	Water Surface Elevation (ft.)	Freeboard (ft.)
2	0.65	0.00	166	95.82	3.61
10	1.05	0.00	507	96.97	2.46
100	1.83	0.91	1,245	99.22	0.21

Notes:

A summary of the pre-development and post-development runoff rates is presented in Table 3, Peak Discharge Rate Comparison Table. Based on the implementation of the stormwater management measures, the peak runoff rates under the post-development conditions will be less than the peak runoff rates for the pre-development conditions.

Table No. 3 - Peak Discharge Rate Comparison Table					
Design Year Storm Event	24-Hour Rainfall (inches)	Pre-Development Peak Runoff Rate (cfs)	Post-Development Peak Runoff Rate (cfs)		
2	3.42	0.25	0.12		
10	5.06	0.83	0.38		
100	8.90	2.49	1.41		

The calculations for pre-development and post-development drainage conditions have been included in Appendix C.

2.5 Erosion & Sediment Control Measures

During construction, the potential for soil erosion and sedimentation will be controlled through the use of temporary soil erosion and sediment control devices and measures. These devices and measures shall be installed and maintained in accordance with the <u>New York State Standards and Specifications for Erosion and Sediment Control</u> dated November 2016 ("Blue Book"). The soil erosion and sediment control (E&SC) measures that will be applied to the site during construction are as follows:

- Install E&SC devices and perform construction in accordance with the construction sequence and design notes;
- Retain existing vegetation where feasible and minimize the amount of land disturbance at any one time;
- Trap sediment on-site prior to discharge from the site;
- Stabilize disturbed areas that will not require further earthwork operations within the required periods specified in the Blue Book, and;
- Implement soil restoration to all disturbed and compacted areas that will be remain unpaved, vegetated and/or landscaped in the post-construction condition in accordance with the requirements in Table 4.6 in the Blue Book, prior to final seeding, landscaping, and mulching.

⁽¹⁾ Freeboard is the difference between the top of the infiltration bed and the water surface elevation. The top of the infiltration bed is elev. 99.43. (i.e. 99.43 – 98.93 = 0.50)

Section 3

Storm Water Management Practice Maintenance

3.1 Long Term Maintenance and Operations

Periodic long-term inspection and maintenance of the Stormwater Management Practices (SMPs) is essential to ensure that the facilities will function as designed. The facility operator, its successors and assigns, shall be responsible for maintaining all onsite SMP components. These components consist of the two drywells and the storm drainage collection system (pipes, drain inlets and manholes).

Comprehensive descriptions of recommended inspection and required maintenance items and intervals for the SMP are provided in the following publications:

- New York State Stormwater Management Design Manual, January 2015.
- "Maintenance Program Guidance", NYSDEC.
- "Reducing the Impacts from Stormwater Runoff from New Development", NYSDEC, Second Edition, April 1993, Chapter 7.
- "Controlling Urban Runoff: A Practical Manual for Planning and Designing Urban BMPs", by Thomas R. Schueler, Department of Environmental Programs, Metropolitan Washington Council of Governments (MWCOG), July 1987, Chapters 3, 4, 5 and 9.

These descriptions are applicable to the selected facilities and provide the foundation for an effective facilities maintenance plan. Descriptions of the facility maintenance for this Project are provided in the following paragraphs:

A. Subsurface Stormwater Detention System

Long term preventative maintenance of subsurface storm water detention systems is essential to the continued effectiveness of the system.

Inspections. The water quality facility should be inspected on an annual basis to ensure that the structure operates in the manner originally intended. When possible, inspections should be conducted during wet weather (minimum 1.0" rainfall in 24 hours) to determine if the facility is meeting the targeted detention times. In particular, the outlet structure should be inspected once every six (6) months for evidence of clogging, or conversely, for too rapid a release. Other problems that should be checked for include: subsidence, the accumulation of sediment around the inlet and/or outlet and the adequacy of upstream/downstream storm pipe system. Inspections should be carried out with as-built plans in hand.

Debris and Litter Removal. Debris, leaves, grass clippings and litter may accumulate near the upstream drain inlets, which convey runoff to the facility and should be removed during regular mowing/maintenance operations. Attention should also be paid to debris that may collect at the outlet control orifice and the debris should be removed regularly.

Structural Repairs and Replacement. Repair or replace as necessary inlet/outlet devices that show signs of deterioration, seepage or failure.

Section 4

Summary and Conclusion

Based on the information presented in this report, the implementation of the proposed Storm Water Management Plan for the Project will meet the design objectives stated in this Report.

Respectfully submitted,

Provident Design Engineering, PLLC

Ralph P. Peragine, P.E. Senior Project Manager New York PE# 064262



Under New York State Education Law Article 145 (Engineering), Section 7209 (2), it is a violation of this law for any person, unless acting under the direction of a Licensed Professional Engineer, to alter this document.

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APPENDIX A - FIGURES

- 1. USDA SOIL SURVEY MAP AND UNIT DESCRIPTION
 - 2. PRE-DEVELOPMENT DRAINAGE AREA MAP
 - 3. POST-DEVELOPMENT DRAINAGE AREA MAP



NRCS

Natural Resources Conservation Service A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

Custom Soil Resource Report for Westchester County, New York

Cabrini of Westchester



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2 053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

The U.S. Department of Agriculture (USDA) prohibits discrimination in all its programs and activities on the basis of race, color, national origin, age, disability, and where applicable, sex, marital status, familial status, parental status, religion, sexual orientation, genetic information, political beliefs, reprisal, or because all or a part of an individual's income is derived from any public assistance program. (Not all prohibited bases apply to all programs.) Persons with disabilities who require

alternative means for communication of program information (Braille, large print, audiotape, etc.) should contact USDA's TARGET Center at (202) 720-2600 (voice and TDD). To file a complaint of discrimination, write to USDA, Director, Office of Civil Rights, 1400 Independence Avenue, S.W., Washington, D.C. 20250-9410 or call (800) 795-3272 (voice) or (202) 720-6382 (TDD). USDA is an equal opportunity provider and employer.

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Westchester County, New York	
KnB—Knickerbocker fine sandy loam, 2 to 8 percent slopes	
Pw—Pompton silt loam, loamy substratum	
RhE—Riverhead loam, 25 to 50 percent slopes	
Ub—Udorthents, smoothed	
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How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

Custom Soil Resource Report

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

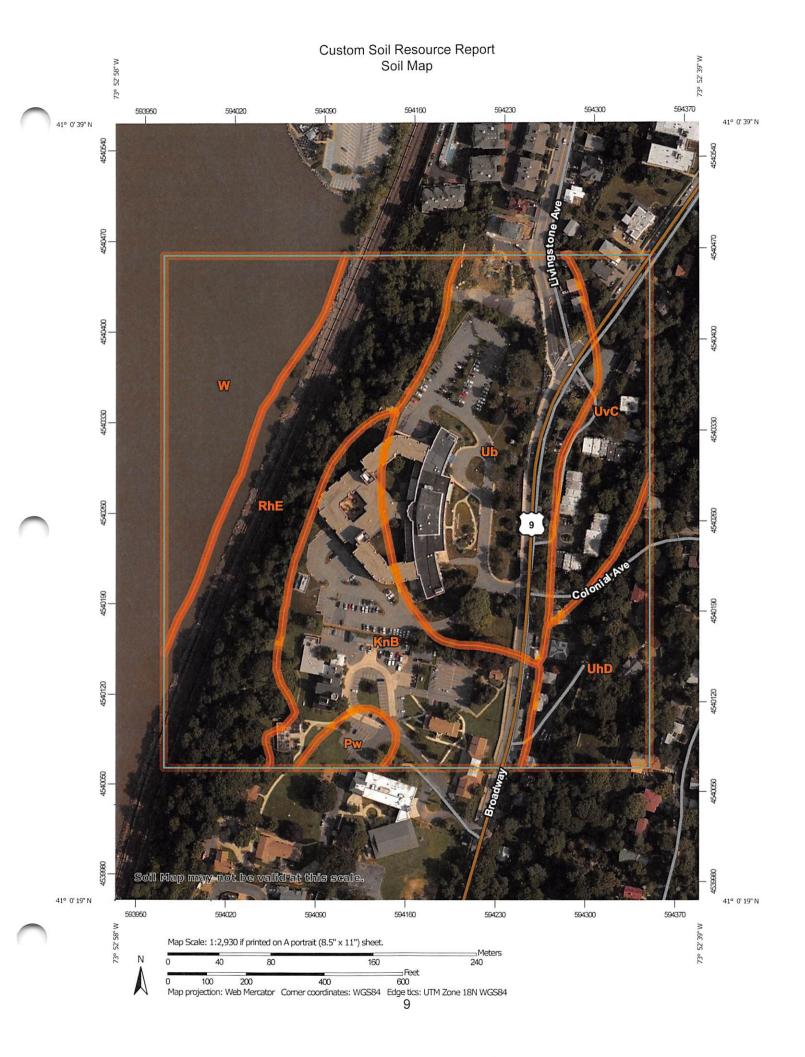
After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

Custom Soil Resource Report

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



MAP LEGEND

Area of Interest (AOI)

Area of Interest (AOI)

Soils

Soil Map Unit Polygons



Soil Map Unit Lines



Soil Map Unit Points

Special Point Features

Blowout (0)

Borrow Pit

簽

Clay Spot

Closed Depression

Gravel Pit

Gravelly Spot Landfill

Lava Flow

Marsh or swamp

Mine or Quarry

Miscellaneous Water

Perennial Water

Rock Outcrop

Saline Spot

Sandy Spot

Severely Eroded Spot Sinkhole

Slide or Slip

Sodic Spot

Spoil Area

Stony Spot Very Stony Spot

0

Wet Spot Other

Δ

Special Line Features

Water Features

Streams and Canals

Transportation

+++

Rails

Interstate Highways

US Routes Major Roads

Local Roads

Background



Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:12,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Westchester County, New York Survey Area Data: Version 14, Sep 3, 2018

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Jul 21, 2014—Aug 27, 2014

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI	
KnB	Knickerbocker fine sandy loam, 2 to 8 percent slopes	6.9	18.6%	
Pw	Pompton silt loam, loamy substratum	0.6	1.6%	
RhE	Riverhead loam, 25 to 50 percent slopes	8.4	22.5%	
Ub	Udorthents, smoothed	9.3	24.9%	
UhD	Urban land-Chariton complex, 15 to 25 percent slopes	3.3	8.9%	
UvC	Urban land-Riverhead complex, 8 to 15 percent slopes	3.5	9.5%	
W	Water	5.2	14.0%	
Totals for Area of Interest		37.2	100.0%	

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not

Custom Soil Resource Report

mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An association is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Westchester County, New York

KnB—Knickerbocker fine sandy loam, 2 to 8 percent slopes

Map Unit Setting

National map unit symbol: bd8s Elevation: 100 to 800 feet

Mean annual precipitation: 46 to 50 inches Mean annual air temperature: 46 to 52 degrees F

Frost-free period: 115 to 215 days

Farmland classification: All areas are prime farmland

Map Unit Composition

Knickerbocker and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Knickerbocker

Setting

Landform: Deltas, terraces

Landform position (two-dimensional): Summit Landform position (three-dimensional): Tread

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Sandy glaciofluvial deposits or deltaic deposits

Typical profile

H1 - 0 to 9 inches: fine sandy loam H2 - 9 to 19 inches: fine sandy loam H3 - 19 to 31 inches: loamy fine sand H4 - 31 to 60 inches: loamy fine sand

Properties and qualities

Slope: 2 to 8 percent

Depth to restrictive feature: More than 80 inches Natural drainage class: Somewhat excessively drained

Capacity of the most limiting layer to transmit water (Ksat): High (1.98 to 5.95

in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Low (about 4.9 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2s

Hydrologic Soil Group: A Hydric soil rating: No

Minor Components

Hinckley

Percent of map unit: 5 percent

Hydric soil rating: No

Riverhead

Percent of map unit: 5 percent

Hydric soil rating: No

Pompton

Percent of map unit: 4 percent

Hydric soil rating: No

Unnamed soils, occasionally flooded

Percent of map unit: 1 percent

Hydric soil rating: No

Pw-Pompton silt loam, loamy substratum

Map Unit Setting

National map unit symbol: bd98

Mean annual precipitation: 46 to 50 inches

Mean annual air temperature: 46 to 52 degrees F

Frost-free period: 115 to 215 days

Farmland classification: All areas are prime farmland

Map Unit Composition

Pompton, loamy substratum, and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Pompton, Loamy Substratum

Setting

Landform: Terraces, valley trains

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Tread

Down-slope shape: Concave Across-slope shape: Linear

Parent material: Loamy over sandy and gravelly glaciofluvial deposits

Typical profile

H1 - 0 to 8 inches: silt loam

H2 - 8 to 26 inches: gravelly fine sandy loam 2C - 26 to 50 inches: very gravelly loamy sand

3C - 50 to 60 inches: gravelly loam

Properties and qualities

Slope: 0 to 3 percent

Depth to restrictive feature: More than 80 inches Natural drainage class: Somewhat poorly drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to

high (0.20 to 1.98 in/hr)

Depth to water table: About 12 to 24 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Moderate (about 8.5 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2w

Hydrologic Soil Group: B/D Hydric soil rating: No

Minor Components

Knickerbocker

Percent of map unit: 3 percent

Hydric soil rating: No

Hinckley

Percent of map unit: 3 percent

Hydric soil rating: No

Riverhead

Percent of map unit: 3 percent

Hydric soil rating: No

Udifluvents

Percent of map unit: 2 percent

Hydric soil rating: No

Fredon

Percent of map unit: 2 percent

Landform: Depressions Hydric soil rating: Yes

Fluvaquents

Percent of map unit: 2 percent

Landform: Flood plains Hydric soil rating: Yes

RhE—Riverhead loam, 25 to 50 percent slopes

Map Unit Setting

National map unit symbol: bd9k

Mean annual precipitation: 46 to 50 inches Mean annual air temperature: 46 to 52 degrees F

Frost-free period: 115 to 215 days

Farmland classification: Not prime farmland

Map Unit Composition

Riverhead and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Riverhead

Setting

Landform: Terraces, deltas

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Riser

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Loamy glaciofluvial deposits overlying stratified sand and gravel

Typical profile

H1 - 0 to 6 inches: loam

H2 - 6 to 25 inches: sandy loam H3 - 25 to 30 inches: loamy sand H4 - 30 to 60 inches: loamy sand

Properties and qualities

Slope: 25 to 50 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): High (1.98 to 5.95

in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Low (about 4.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7e

Hydrologic Soil Group: A Hydric soil rating: No

Minor Components

Pompton

Percent of map unit: 5 percent

Hydric soil rating: No

Charlton

Percent of map unit: 4 percent

Hydric soil rating: No

Knickerbocker

Percent of map unit: 3 percent

Hydric soil rating: No

Hinckley

Percent of map unit: 3 percent

Hydric soil rating: No

Ub—Udorthents, smoothed

Map Unit Setting

National map unit symbol: bd7f Elevation: 50 to 2,400 feet

Mean annual precipitation: 46 to 50 inches Mean annual air temperature: 46 to 52 degrees F

Frost-free period: 115 to 215 days

Farmland classification: Not prime farmland

Map Unit Composition

Udorthents, smoothed, and similar soils: 80 percent

Minor components: 20 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Udorthents, Smoothed

Typical profile

H1 - 0 to 4 inches: gravelly loam H2 - 4 to 70 inches: very gravelly loam

Properties and qualities

Slope: 0 to 8 percent

Depth to restrictive feature: 40 to 60 inches to lithic bedrock

Natural drainage class: Moderately well drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.06 to 5.95 in/hr)

Depth to water table: About 18 to 48 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum in profile: 15 percent Available water storage in profile: Low (about 4.6 inches)

Minor Components

Udorthents, wet substratum

Percent of map unit: 5 percent

Hydric soil rating: No

Urban land

Percent of map unit: 5 percent Hydric soil rating: Unranked

Leicester

Percent of map unit: 2 percent

Hydric soil rating: No

Hollis

Percent of map unit: 2 percent

Hydric soil rating: No

Charlton

Percent of map unit: 2 percent

Hydric soil rating: No

Riverhead

Percent of map unit: 2 percent

Hydric soil rating: No

Sun

Percent of map unit: 2 percent Landform: Depressions

Hydric soil rating: Yes

UhD—Urban land-Charlton complex, 15 to 25 percent slopes

Map Unit Setting

National map unit symbol: 2wh1n

Elevation: 20 to 470 feet

Mean annual precipitation: 36 to 71 inches

Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Not prime farmland

Map Unit Composition

Urban land: 40 percent

Charlton and similar soils: 35 percent Minor components: 25 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Urban Land

Typical profile

M - 0 to 10 inches: cemented material

Properties and qualities

Slope: 15 to 25 percent

Depth to restrictive feature: 0 inches to manufactured layer

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Very low (0.00 to 0.00

in/hr)

Available water storage in profile: Very low (about 0.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8

Hydrologic Soil Group: D Hydric soil rating: Unranked

Description of Charlton

Setting

Landform: Ridges, hills, ground moraines
Landform position (two-dimensional): Backslope
Landform position (three-dimensional): Side slope

Down-slope shape: Linear, convex Across-slope shape: Convex

Parent material: Coarse-loamy melt-out till derived from gneiss, granite, and/or

schist

Typical profile

Ap - 0 to 7 inches: fine sandy loam

Bw - 7 to 22 inches: gravelly fine sandy loam C - 22 to 65 inches: gravelly fine sandy loam

Properties and qualities

Slope: 15 to 25 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Well drained

Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Salinity, maximum in profile: Nonsaline (0.0 to 1.9 mmhos/cm) Available water storage in profile: Moderate (about 6.9 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4e

Hydrologic Soil Group: B Hydric soil rating: No

Minor Components

Leicester

Percent of map unit: 8 percent

Landform: Depressions, drainageways, ground moraines, hills Landform position (two-dimensional): Toeslope, footslope Landform position (three-dimensional): Base slope

Down-slope shape: Linear, concave

Across-slope shape: Concave

Hydric soil rating: Yes

Chatfield

Percent of map unit: 7 percent

Landform: Hills, ridges

Landform position (two-dimensional): Shoulder, summit, backslope Landform position (three-dimensional): Crest, side slope, nose slope

Down-slope shape: Convex

Across-slope shape: Linear, convex

Hydric soil rating: No

Udorthents

Percent of map unit: 5 percent

Landform: Ridges

Landform position (three-dimensional): Tread

Down-slope shape: Linear, convex Across-slope shape: Linear, convex

Hydric soil rating: No

Sutton

Percent of map unit: 5 percent Landform: Hills, ground moraines

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

UvC-Urban land-Riverhead complex, 8 to 15 percent slopes

Map Unit Setting

National map unit symbol: bd7x

Mean annual precipitation: 46 to 50 inches Mean annual air temperature: 46 to 52 degrees F

Frost-free period: 115 to 215 days

Farmland classification: Not prime farmland

Map Unit Composition

Urban land: 50 percent

Riverhead and similar soils: 25 percent

Minor components: 25 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Riverhead

Setting

Landform: Deltas, terraces

Landform position (two-dimensional): Shoulder Landform position (three-dimensional): Tread

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Loamy glaciofluvial deposits overlying stratified sand and gravel

Typical profile

H1 - 0 to 6 inches: loam

H2 - 6 to 25 inches: sandy loam H3 - 25 to 30 inches: loamy sand H4 - 30 to 60 inches: loamy sand

Properties and qualities

Slope: 8 to 15 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): High (1.98 to 5.95

in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Low (about 4.4 inches)

Minor Components

Hinckley

Percent of map unit: 5 percent

Hydric soil rating: No

Pompton

Percent of map unit: 5 percent

Hydric soil rating: No

Udorthents

Percent of map unit: 5 percent

Hydric soil rating: No

Knickerbocker

Percent of map unit: 5 percent

Hydric soil rating: No

Charlton

Percent of map unit: 3 percent

Hydric soil rating: No

Fluvaquents

Percent of map unit: 1 percent

Landform: Flood plains Hydric soil rating: Yes

Udifluvents

Percent of map unit: 1 percent

Hydric soil rating: No

W-Water

Map Unit Setting

National map unit symbol: bd7z

Mean annual precipitation: 46 to 50 inches Mean annual air temperature: 46 to 52 degrees F

Frost-free period: 115 to 215 days

Farmland classification: Not prime farmland

Map Unit Composition

Water: 100 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Soil Information for All Uses

Soil Reports

The Soil Reports section includes various formatted tabular and narrative reports (tables) containing data for each selected soil map unit and each component of each unit. No aggregation of data has occurred as is done in reports in the Soil Properties and Qualities and Suitabilities and Limitations sections.

The reports contain soil interpretive information as well as basic soil properties and qualities. A description of each report (table) is included.

Soil Erosion

This folder contains a collection of tabular reports that present soil erosion factors and groupings. The reports (tables) include all selected map units and components for each map unit. Soil erosion factors are soil properties and interpretations used in evaluating the soil for potential erosion. Example soil erosion factors can include K factor for the whole soil or on a rock free basis, T factor, wind erodibility group and wind erodibility index.

RUSLE2 Related Attributes

This report summarizes those soil attributes used by the Revised Universal Soil Loss Equation Version 2 (RUSLE2) for the map units in the selected area. The report includes the map unit symbol, the component name, and the percent of the component in the map unit. Soil property data for each map unit component include the hydrologic soil group, erosion factors Kf for the surface horizon, erosion factor T, and the representative percentage of sand, silt, and clay in the mineral surface horizon. Missing surface data may indicate the presence of an organic surface layer.

Report—RUSLE2 Related Attributes

Soil properties and interpretations for erosion runoff calculations. The surface mineral horizon properties are displayed. Organic surface horizons are not displayed.

RUSLE2 Related Attributes-Westchester County, New York								
Map symbol and soil name	Pct. of	Slope	Hydrologic group	Kf	T factor	Representative value		
	map unit	length (ft)				% Sand	% Silt	% Clay
KnB—Knickerbocker fine sandy loam, 2 to 8 percent slopes								
Knickerbocker	85	_	А	.17	2	64.6	25.4	10.0
Pw—Pompton silt loam, loamy substratum								
Pompton, loamy substratum	85	_	B/D	.37	5	30.7	57.3	12.0
RhE—Riverhead loam, 25 to 50 percent slopes								
Riverhead	85	-	А	.28	3	47.9	40.1	12.0
Ub—Udorthents, smoothed								
Udorthents, smoothed	80	_	В	.32	3	42.1	45.9	12.0
UhD—Urban land-Charlton complex, 15 to 25 percent slopes								
Urban land	40	69	D	_	_	_	_	_
Charlton	35	49	В	.24	5	57.0	34.0	9.0
UvC—Urban land-Riverhead complex, 8 to 15 percent slopes								
Riverhead	25	_	A	.28	3	47.9	40.1	12.0

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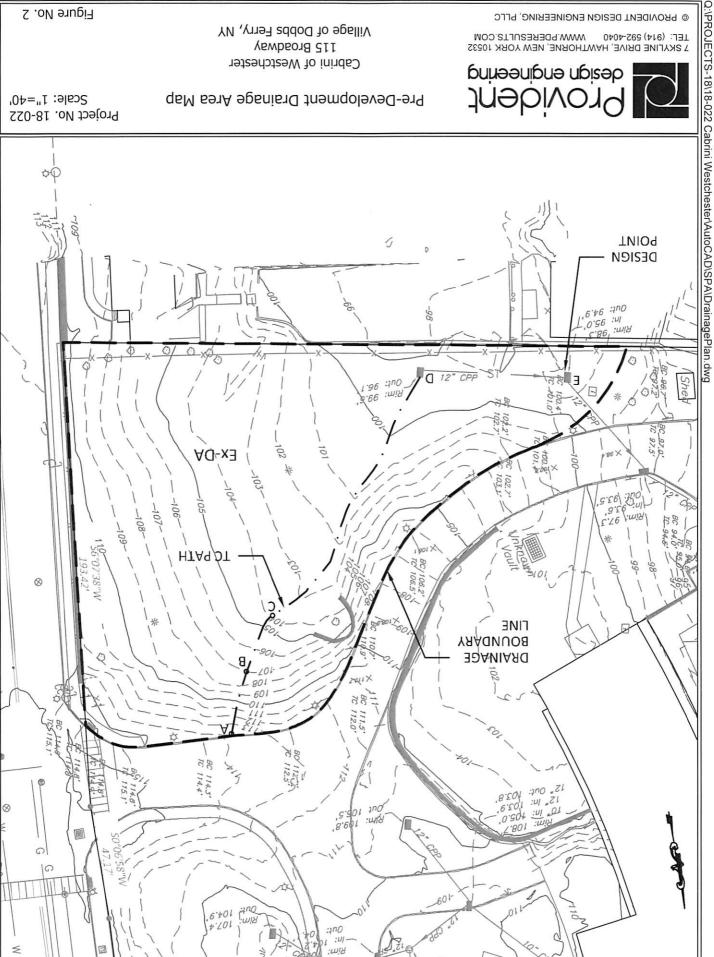


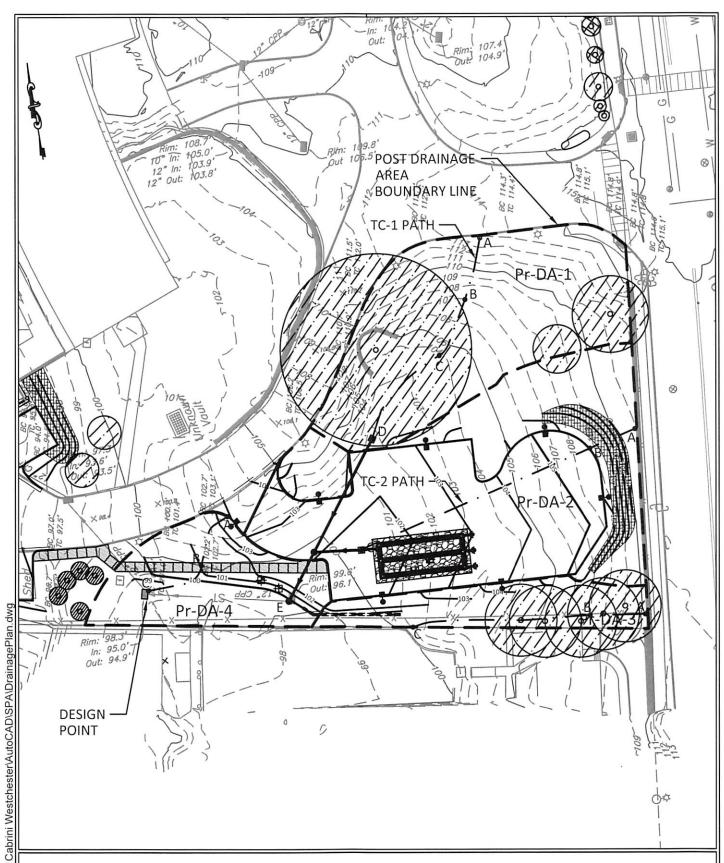
Figure No. 2

Pre-Development Drainage Area Map

Village of Dobbs Ferry, NY 115 Broadway Cabrini of Westchester

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Post-Development Drainage Area Map

Cabrini of Westcheater 115 Broadway Village of Dobbs Ferry, NY Project No. 18-022 Scale: 1"=40'

Figure No. 3

APPENDIX B - SUBSURFACE INVESTIGATION TEST PIT LOGS INFILTRATION TESTING DATA SHEETS



7 Skyline Drive Hawthorne, New York 10532 Phone 914-592-4040

END DATE

TEST PIT LOG

TEST PIT: TP-1 SHEET: 1 OF 2

PROJECT NO. 18-022 INSPECTOR C. Hanzlik, K. Murphy EXCAVATOR Carmine Giuliano

Depth to Groundwater Depth to Bedrock

10/18/2018		10/18/2018 N/A	N/A
		DESCRIPTION OF SOILS	REMARKS
	_3	DESCRIPTION OF SOLES	(PID, STAINING, ODORS, ETC.)
	BOI	(SAA = Same As Above)	FP = Free Product
<u> </u>	ΥM	(SILL SHIRLE HOVE)	N/S = No Staining, N/O = No odors
DEPTH (ft)	S	f-fine m-medium c-coarse	SO = Slight Odor, MO = Moderate Odor
DE	USCS SYMBOL	lt - light dk - dark tr - trace ltl - little	STO = Strong Odor
1.0			N/S, N/O
2.0			
3.0			
5.0	SM	Lt Brown m-f SAND, w/silt, moist	N/S, N/O
6.0			
7.0		End of Test Pit at 7.0' bgs - backfilled	



7 Skyline Drive Hawthorne, New York 10532 Phone 914-592-4040

TEST PIT LOG

TEST PIT: TP-2 SHEET: 2 OF 2

 JOB NAME/ CLIENT
 PROJECT NO.

 Cabrini of Westchester
 18-022

 ADDRESS
 INSPECTOR
 EXCAVATOR

 115 Broadway, Dobbs Ferry, NY 10522
 C. Hanzlik, K. Murphy
 Carmine Giulianc

 START DATE
 END DATE
 Depth to Groundwater
 Depth to Bedrock

 10/18/2018
 10/18/2018
 N/A
 N/A

10/18/2018		10/18/2018 N/A	N/A
		DESCRIPTION OF SOILS	REMARKS
1 1		Discini IIo. or soils	(PID, STAINING, ODORS, ETC.)
_	BO	(SAA = Same As Above)	FP = Free Product
5	X.N	, and a second of	N/S = No Staining, N/O = No odors
DEPTH (ft)	SS	f - fine m - medium c - coarse	SO = Slight Odor, MO = Moderate Odor
DE	USCS SYMBOL	lt - light dk - dark tr - trace ltl - little	STO = Strong Odor
		Dk Brown to Black Topsoil w/organics	N/S, N/O
1 1		on brown to black ropoon worganies	,
1.0			
1 1			
1 1			
2.0			
3.0			
1 1			
1 1			
4.0	SM	Dk Brown m-f SAND, w/silt, moist	N/S, N/O
1.0	5.11	DR BIOWH III 1 57 th O, W/sitt, moist	,
1 1			
1 1			
1 1			
5.0			
5.0			
1			
6.0			
7.0			
7.0		End of Test Pit at 7.0' bgs - backfilled	
		Lind of Post III at 7.0 ogs - odekimed	
\vdash			
H -			

TEST DATE
1' TO 7' LT BROWN M-F SAND, W/SILT, MOIST TP-2 0 TO 1' DK BROWN TO BLACK TOPSOIL W/ORGAI
TP-2 0 TO 1' DK BROWN TO BLACK TOPSOIL W/ORGA
U TO THE LET DROUBLAGE CAME WIGHT MOIST
l' TO 7' LT BROWN M-F SAND, W/SILT, MOIST
BGS - BELOW GROUND SURFACE

7	INFILTRA	ATION TEST DATA TABLE
	TEST DATE	OCTOBER 19, 2018
7	TEST NO.	NFILTRATION DESIGN RATE
Ī	PT-1	3.30 MIN./INCH
7	PT-2	3.75 MIN./INCH
īcs		

Provident Design Engineering, PLLC DESIGN DATA SHEET – STORMWATER INFILTRATION TESTING

Project Name: Cabrini of Westchester Nursing Home							
Owner: Cabrini of Westchester	Addre	ss: 115 Broadw	ay, Dobbs Ferr	ry, NY 10522			
Located at (Street): 115 Broadway	7	Sec. 0	Block: 0	Lot: 00			
Dobbs Ferry, I	VY						
(Indicate nearest cross street): N/A							
Municipality: Dobbs Ferry (V)	Count	y: Westchester	Watershed: H	ludson River			

<u>Pre-Soak Date</u>: 10.18.2018 <u>Run Date</u>: 10.19.2018

	CLOC	K TIME	-	INFILTRATION (Test Hole Depth @ 84 inches bgs)			
Run No.	Start	Stop	Elapsed Time (Min.)	_	Water from VC Casing Stop Inches	Water Level Drop (Inches)	Soil Rate Min/In Drop
			HOL	E NUMBE	R – PT-1		
1	10:38A	11:38A	60	72	94(1)	22	2.72
2	11:30A	12:39P	60	72	90	18	3.33
3	12:40P	1:40P	60	72	90	18	3.33
4				_			
HOLE NUMBER – PT-2							
1	10:50A	11:50A	60	66	88 ⁽²⁾	22	2.72
2	11:50A	12:50P	60	66	83	17	3.53
3	12:50P	1:50P	60	66	82	16	3.75
4							
			HOL	LE NUMBE	R –		· -
1							
2							
3							
4							
		T	HOI	E NUMBE	R –		
1							_
2							
3							
4							

Note:

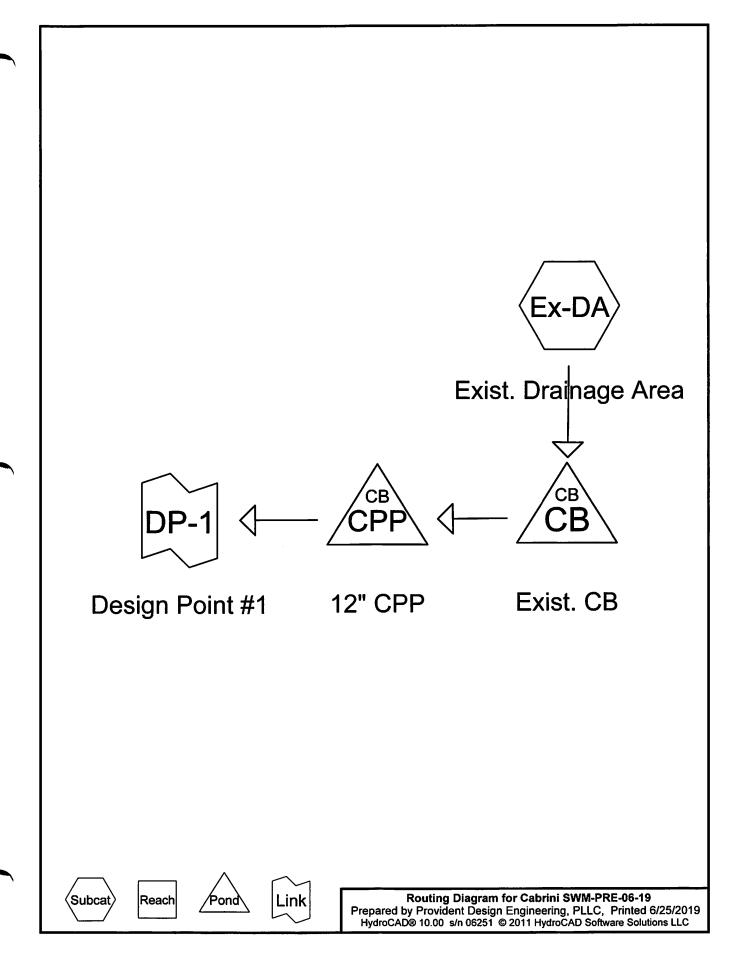
- 1. Overall depth of PVC casing 96 inches.
- 2. Overall depth of PVC casing 90 inches.

Witnessed by: Ken Murphy - Provident Design Engineering, PLLC (PDE)

Reviewed by: Ralph P. Peragine, P.E., PDE

APPENDIX C STORM WATER MANAGEMENT CALCULATIONS

APPENDIX C-1 PRE-DEVELOPMENT CALCULATIONS



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Pre-development SWM Calculations NY-DobbsFerry 24-hr S1 2-yr 2-yr Rainfall=3.42"
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Page 2

Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points
Runoff by SCS TR-20 method, UH=SCS
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment Ex-DA: Exist. Drainage Area

Runoff Area=25,166 sf 0.00% Impervious Runoff Depth=0.54" Flow Length=172' Tc=6.0 min CN=61 Runoff=0.25 cfs 1,127 cf

Pond CB: Exist. CB

Peak Elev=96.35' Inflow=0.25 cfs 1,127 cf Outflow=0.25 cfs 1,127 cf

Pond CPP: 12" CPP

Peak Elev=96.35' Inflow=0.25 cfs 1,127 cf 12.0" Round Culvert n=0.013 L=59.5' S=0.0202'/' Outflow=0.25 cfs 1,127 cf

Link DP-1: Design Point #1

Inflow=0.25 cfs 1,127 cf Primary=0.25 cfs 1,127 cf

Total Runoff Area = 25,166 sf Runoff Volume = 1,127 cf Average Runoff Depth = 0.54" 100.00% Pervious = 25,166 sf 0.00% Impervious = 0 sf

Page 3

Summary for Subcatchment Ex-DA: Exist. Drainage Area

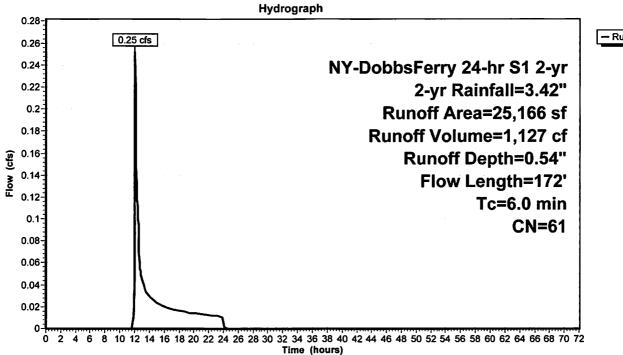
Runoff 0.25 cfs @ 12.06 hrs, Volume= 1,127 cf, Depth= 0.54"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NY-DobbsFerry 24-hr S1 2-yr 2-yr Rainfall=3.42"

A	rea (sf)	CN D	escription						
	25,166	61 >7	1 >75% Grass cover, Good, HSG B						
	25,166 100.00% Pervious Area								
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
1.7	27	0.2600	0.26	, , , ,	Sheet Flow, AB				
0.1	26	0.1150	5.09		Grass: Dense n= 0.240 P2= 3.50" Shallow Concentrated Flow, BC Grassed Waterway Kv= 15.0 fps				
0.7	119	0.0370	2.89		Shallow Concentrated Flow, CD Grassed Waterway Kv= 15.0 fps				

2.5 172 Total, Increased to minimum Tc = 6.0 min

Subcatchment Ex-DA: Exist. Drainage Area



- Runoff

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Page 4

- Inflow

- Primary

Summary for Pond CB: Exist. CB

Inflow Area = 25,166 sf, 0.00% Impervious, Inflow Depth = 0.54" for 2-yr event

Inflow = 0.25 cfs @ 12.06 hrs, Volume= 1,127 cf

Outflow = 0.25 cfs @ 12.06 hrs, Volume= 1,127 cf, Atten= 0%, Lag= 0.0 min

Primary = 0.25 cfs @ 12.06 hrs, Volume= 1,127 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 96.35' @ 12.06 hrs

Flood Elev= 99.60'

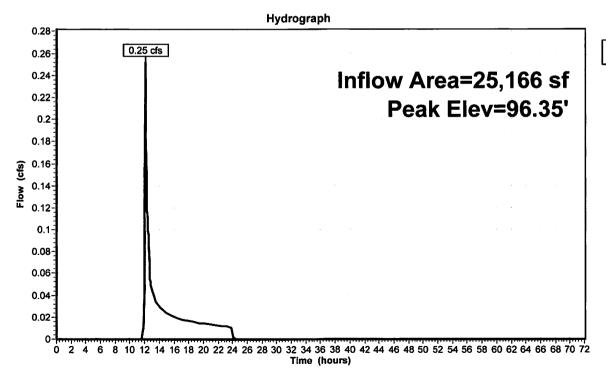
Device	Routing	Invert	Outlet Devices
#1	Primary	96.10'	12.0" Round Culvert L= 59.5' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 96.10' / 94.90' S= 0.0202 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#2	Primary	99.50'	24.0" x 36.0" Horiz. Orifice/Grate C= 0.600 Limited to weir flow at low heads

Primary OutFlow Max=0.24 cfs @ 12.06 hrs HW=96.34' (Free Discharge)

1=Culvert (inlet Controls 0.24 cfs @ 1.66 fps)

-2=Orifice/Grate (Controls 0.00 cfs)

Pond CB: Exist. CB



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Pre-development SWM Calculations
NY-DobbsFerry 24-hr S1 2-yr 2-yr Rainfall=3.42"
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Summary for Pond CPP: 12" CPP

Inflow Area =

25,166 sf, 0.00% Impervious, Inflow Depth = 0.54" for 2-yr event

Inflow =

0.25 cfs @ 12.06 hrs, Volume=

1,127 cf

Outflow =

0.25 cfs @ 12.06 hrs, Volume=

1,127 cf, Atten= 0%, Lag= 0.0 min

Primary

0.25 cfs @ 12.06 hrs, Volume=

1,127 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

96.10'

Peak Elev= 96.35' @ 12.06 hrs

Flood Elev= 98.30'

Device Routing #1 Primary

Invert Outlet Devices

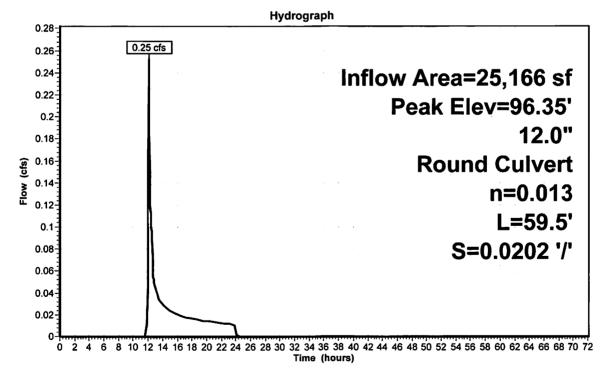
12.0" Round Culvert L= 59.5' Square-edged headwall, Ke= 0.500

Inlet / Outlet Invert= 96.10' / 94.90' S= 0.0202 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=0.24 cfs @ 12.06 hrs HW=96.34' (Free Discharge)

1=Culvert (Inlet Controls 0.24 cfs @ 1.66 fps)

Pond CPP: 12" CPP





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Summary for Link DP-1: Design Point #1

Inflow Area =

25,166 sf, 0.00% Impervious, Inflow Depth = 0.54" for 2-yr event

Inflow

0.25 cfs @ 12.06 hrs, Volume=

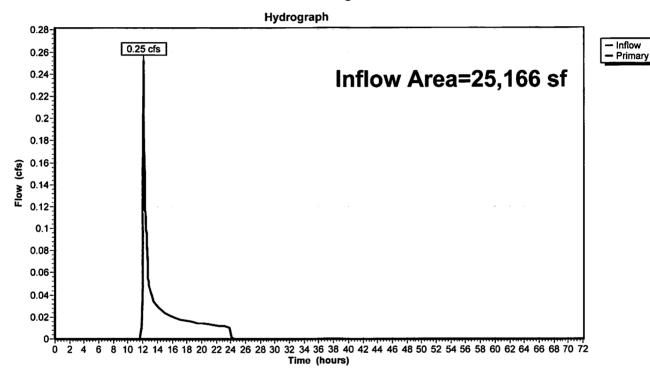
1,127 cf

Primary 0.25 cfs @ 12.06 hrs, Volume=

1,127 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link DP-1: Design Point #1



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Pre-development SWM Calculations

NY-DobbsFerry 24-hr S1 10-yr 10-yr Rainfall=5.06"

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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points
Runoff by SCS TR-20 method, UH=SCS
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment Ex-DA: Exist. Drainage Area

Runoff Area=25,166 sf 0.00% Impervious Runoff Depth=1.41" Flow Length=172' Tc=6.0 min CN=61 Runoff=0.83 cfs 2,947 cf

Pond CB: Exist. CB

Peak Elev=96.57' Inflow=0.83 cfs 2,947 cf Outflow=0.83 cfs 2,947 cf

Pond CPP: 12" CPP

Peak Elev=96.57' Inflow=0.83 cfs 2,947 cf 12.0" Round Culvert n=0.013 L=59.5' S=0.0202 '/' Outflow=0.83 cfs 2,947 cf

Link DP-1: Design Point #1

Inflow=0.83 cfs 2,947 cf Primary=0.83 cfs 2,947 cf

Total Runoff Area = 25,166 sf Runoff Volume = 2,947 cf Average Runoff Depth = 1.41"

100.00% Pervious = 25,166 sf 0.00% Impervious = 0 sf

Page 8

Summary for Subcatchment Ex-DA: Exist. Drainage Area

Runoff = 0.83 cfs @ 12.05 hrs, Volume=

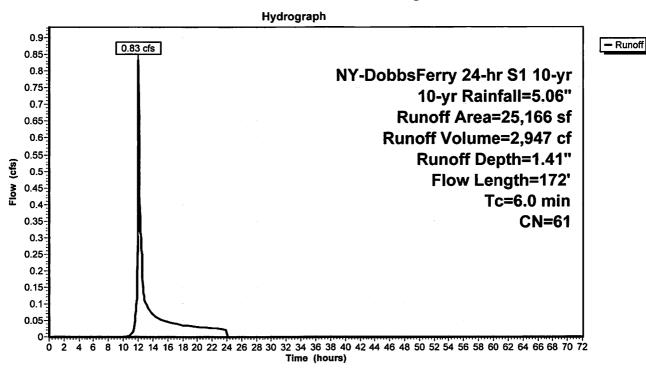
2,947 cf, Depth= 1.41"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NY-DobbsFerry 24-hr S1 10-yr 10-yr Rainfall=5.06"

A	rea (sf)	CN De	escription		
	25,166	61 >7	75% Grass	cover, Goo	d, HSG B
	25,166 100.00% Pervious Area			vious Area	
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.7	27	0.2600	0.26	· · · · · ·	Sheet Flow, AB Grass: Dense n= 0.240 P2= 3.50"
0.1	26	0.1150	5.09		Shallow Concentrated Flow, BC Grassed Waterway Kv= 15.0 fps
0.7	119	0.0370	2.89		Shallow Concentrated Flow, CD Grassed Waterway Kv= 15.0 fps

2.5 172 Total, Increased to minimum Tc = 6.0 min

Subcatchment Ex-DA: Exist. Drainage Area



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Page 9

- Inflow

- Primary

Summary for Pond CB: Exist. CB

Inflow Area = 25,166 sf, 0.00% Impervious, Inflow Depth = 1.41" for 10-yr event

Inflow = 0.83 cfs @ 12.05 hrs, Volume= 2,947 cf

Outflow = 0.83 cfs @ 12.05 hrs, Volume= 2,947 cf, Atten= 0%, Lag= 0.0 min

Primary = 0.83 cfs @ 12.05 hrs, Volume= 2,947 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 96.57' @ 12.05 hrs

Flood Elev= 99.60'

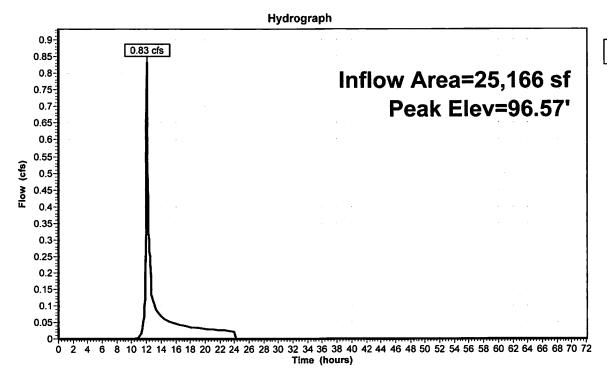
Device	Routing	Invert	Outlet Devices
#1	Primary	96.10'	12.0" Round Culvert L= 59.5' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 96.10' / 94.90' S= 0.0202 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#2	Primary	99.50'	24.0" x 36.0" Horiz. Orifice/Grate C= 0.600 Limited to weir flow at low heads

Primary OutFlow Max=0.83 cfs @ 12.05 hrs HW=96.56' (Free Discharge)

-1=Culvert (Inlet Controls 0.83 cfs @ 2.32 fps)

-2=Orifice/Grate (Controls 0.00 cfs)

Pond CB: Exist. CB



Pre-development SWM Calculations NY-DobbsFerry 24-hr S1 10-yr 10-yr Rainfall=5.06" Printed 6/25/2019 1:28:58 PM

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Summary for Pond CPP: 12" CPP

Inflow Area = 25,166 sf, 0.00% Impervious, Inflow Depth = 1.41" for 10-yr event

Inflow 0.83 cfs @ 12.05 hrs, Volume= 2,947 cf

Outflow 0.83 cfs @ 12.05 hrs, Volume= 2,947 cf, Atten= 0%, Lag= 0.0 min

Primary 0.83 cfs @ 12.05 hrs, Volume= 2,947 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

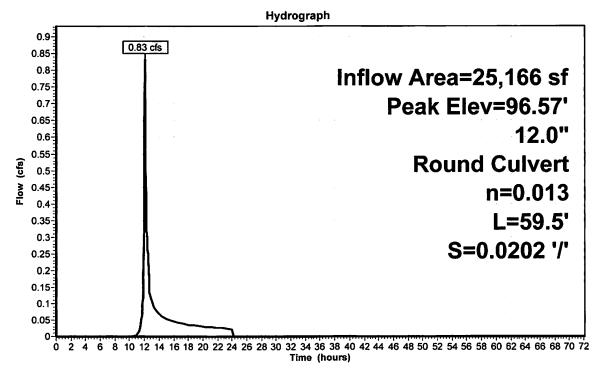
Peak Elev= 96.57' @ 12.05 hrs

Flood Elev= 98.30'

Device	Routing	Invert	Outlet Devices
#1	Primary	96.10'	12.0" Round Culvert L= 59.5' Square-edged headwall, Ke= 0.500 Inlet / Outlet Invert= 96.10' / 94.90' S= 0.0202 '/' Cc= 0.900
			n= 0.013 Corrugated PF, smooth interior. Flow Area= 0.79 sf

Primary OutFlow Max=0.83 cfs @ 12.05 hrs HW=96.56' (Free Discharge) T_1=Culvert (Inlet Controls 0.83 cfs @ 2.32 fps)

Pond CPP: 12" CPP





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- Inflow

Primary

Summary for Link DP-1: Design Point #1

Inflow Area =

Primary

25,166 sf, 0.00% Impervious, Inflow Depth = 1.41" for 10-yr event

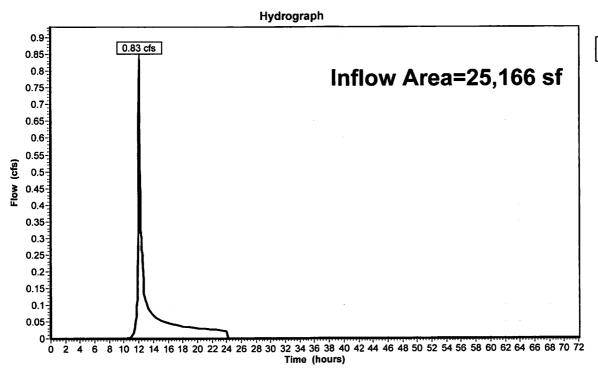
Inflow =

0.83 cfs @ 12.05 hrs, Volume= 0.83 cfs @ 12.05 hrs, Volume= 2,947 cf

2,947 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link DP-1: Design Point #1



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Pre-development SWM Calculations NY-DobbsFerry 24-hr S1 100-yr 100-yr Rainfall=8.90" Printed 6/25/2019 1:28:58 PM

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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points Runoff by SCS TR-20 method, UH=SCS Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment Ex-DA: Exist. Drainage Area

Runoff Area=25,166 sf 0.00% Impervious Runoff Depth=4.14" Flow Length=172' Tc=6.0 min CN=61 Runoff=2.49 cfs 8,692 cf

Pond CB: Exist. CB

Peak Elev=97.03' Inflow=2.49 cfs 8,692 cf Outflow=2.49 cfs 8,692 cf

Pond CPP: 12" CPP

Peak Elev=97.03' Inflow=2.49 cfs 8,692 cf 12.0" Round Culvert n=0.013 L=59.5' S=0.0202'/' Outflow=2.49 cfs 8,692 cf

Link DP-1: Design Point #1

Inflow=2.49 cfs 8,692 cf Primary=2.49 cfs 8,692 cf

Total Runoff Area = 25,166 sf Runoff Volume = 8,692 cf Average Runoff Depth = 4.14" 100.00% Pervious = 25,166 sf 0.00% Impervious = 0 sf

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Summary for Subcatchment Ex-DA: Exist. Drainage Area

Runoff 2.49 cfs @ 12.05 hrs, Volume= 8,692 cf, Depth= 4.14"

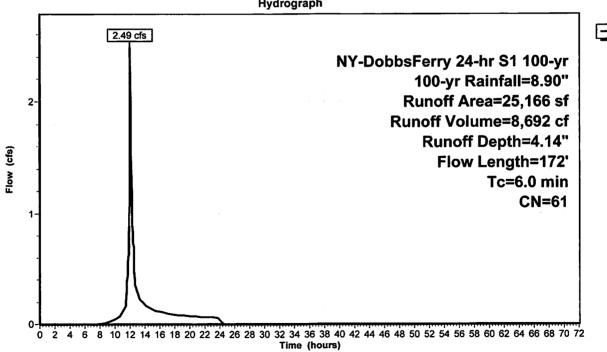
Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NY-DobbsFerry 24-hr S1 100-yr 100-yr Rainfall=8.90"

A	rea (sf)	CN De	escription		
	25,166	61 >7	>75% Grass cover, Good, HSG B		
	25,166 100.00% Pervious Area				
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.7	27	0.2600	0.26		Sheet Flow, AB Grass: Dense n= 0.240 P2= 3.50"
0.1	26	0.1150	5.09		Shallow Concentrated Flow, BC Grassed Waterway Kv= 15.0 fps
0.7	119	0.0370	2.89		Shallow Concentrated Flow, CD Grassed Waterway Kv= 15.0 fps

2.5 172 Total, Increased to minimum Tc = 6.0 min

Subcatchment Ex-DA: Exist. Drainage Area

Hydrograph



- Runoff

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Summary for Pond CB: Exist. CB

25,166 sf, 0.00% Impervious, Inflow Depth = 4.14" for 100-yr event Inflow Area =

Inflow 2.49 cfs @ 12.05 hrs, Volume= 8,692 cf

Outflow = 2.49 cfs @ 12.05 hrs, Volume= 8,692 cf, Atten= 0%, Lag= 0.0 min

Primary = 2.49 cfs @ 12.05 hrs, Volume= 8.692 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Peak Elev= 97.03' @ 12.05 hrs

Flood Elev= 99.60'

Device	Routing	Invert	Outlet Devices
#1	Primary	96.10'	12.0" Round Culvert L= 59.5' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 96.10' / 94.90' S= 0.0202 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#2	Primary	99.50'	24.0" x 36.0" Horiz. Orifice/Grate C= 0.600 Limited to weir flow at low heads

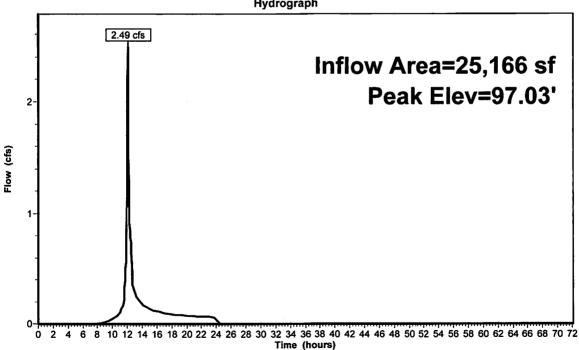
Primary OutFlow Max=2.45 cfs @ 12.05 hrs HW=97.01' (Free Discharge)

-1=Culvert (Inlet Controls 2.45 cfs @ 3.26 fps)

2=Orifice/Grate (Controls 0.00 cfs)

Pond CB: Exist. CB

Hydrograph





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Pre-development SWM Calculations NY-DobbsFerry 24-hr S1 100-yr 100-yr Rainfall=8.90"
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Summary for Pond CPP: 12" CPP

Inflow Area = 25,166 sf, 0.00% Impervious, Inflow Depth = 4.14" for 100-yr event

Inflow = 2.49 cfs @ 12.05 hrs, Volume= 8,692 cf

Outflow = 2.49 cfs @ 12.05 hrs, Volume= 8,692 cf, Atten= 0%, Lag= 0.0 min

Primary = 2.49 cfs @ 12.05 hrs, Volume= 8,692 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Peak Elev= 97.03' @ 12.05 hrs

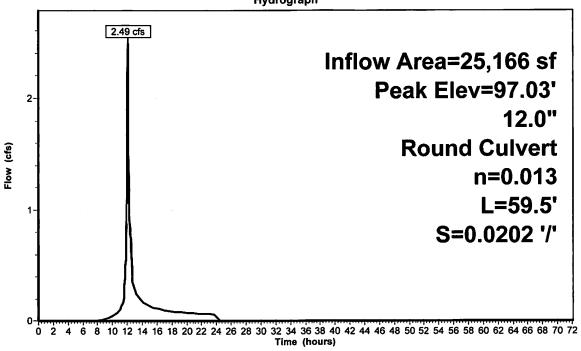
Flood Elev= 98.30'

Device	Routing	Invert	Outlet Devices	
#1	Primary	96.10'	12.0" Round Culvert L= 59.5' Square-edged headwall, Ke= 0.500	
			Inlet / Outlet Invert= 96.10' / 94.90' S= 0.0202 '/' Cc= 0.900	
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf	

Primary OutFlow Max=2.45 cfs @ 12.05 hrs HW=97.01' (Free Discharge) 1=Culvert (Inlet Controls 2.45 cfs @ 3.26 fps)

Pond CPP: 12" CPP

Hydrograph





Pre-development SWM Calculations
NY-DobbsFerry 24-hr S1 100-yr 100-yr Rainfall=8.90"
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Summary for Link DP-1: Design Point #1

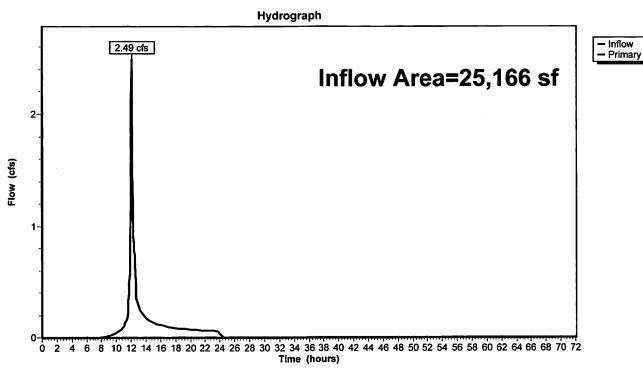
Inflow Area = 25,166 sf, 0.00% Impervious, Inflow Depth = 4.14" for 100-yr event

Inflow = 2.49 cfs @ 12.05 hrs, Volume= 8,692 cf

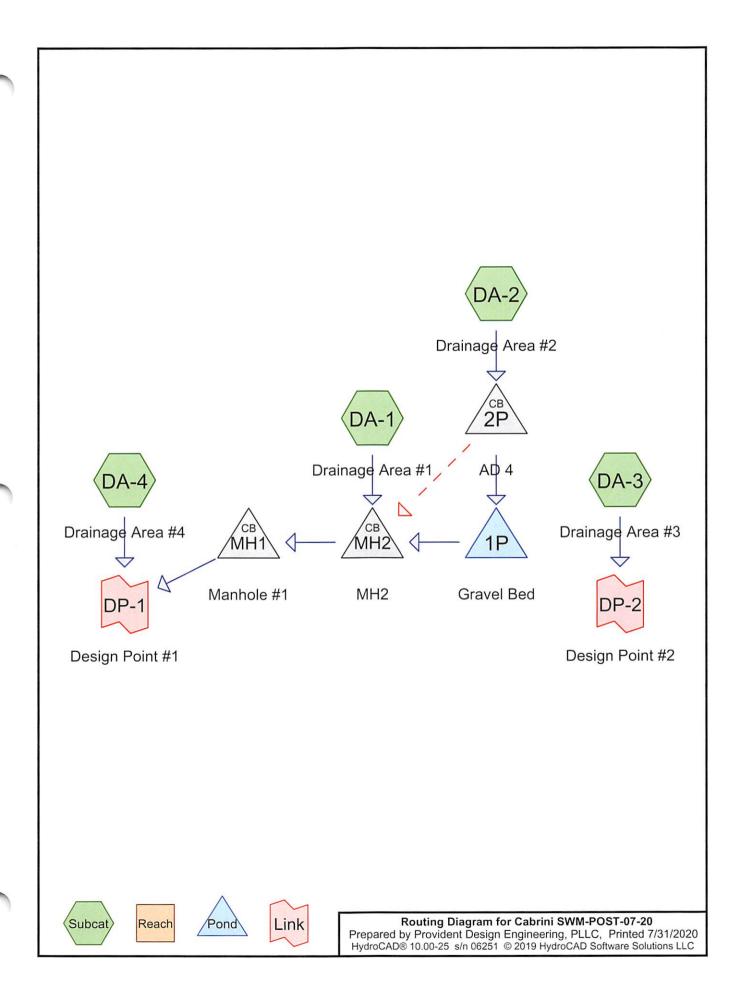
Primary = 2.49 cfs @ 12.05 hrs, Volume= 8,692 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link DP-1: Design Point #1



APPENDIX C-2 POST-DEVELOPMENT CALCULATIONS



Q:\PROJECTS-18\18-022 Cabrini Westchester\SWM\ Cabrini SWM-POST-07-20

Pond MH2: MH2

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Appendix C August 2020 NY-DobbsFerry 24-hr S1 2-yr Rainfall=3.42" Printed 7/31/2020 1:54:00 PM

Page 2

Time span=0.00-48.00 hrs, dt=0.05 hrs, 961 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment DA-1: Drainage Area #1 Runoff Area=7,576 sf 0.00% Impervious Runoff Depth=0.54"

Flow Length=175' Tc=6.0 min CN=61 Runoff=0.08 cfs 339 cf

Subcatchment DA-2: Drainage Area #2

Runoff Area=11,973 sf 62.60% Impervious Runoff Depth=1.87"

Flow Length=149' Tc=6.0 min CN=84 Runoff=0.65 cfs 1,864 cf

Subcatchment DA-3: Drainage Area #3

Runoff Area=2,275 sf 0.00% Impervious Runoff Depth=0.54"

Flow Length=99' Tc=6.0 min CN=61 Runoff=0.02 cfs 102 cf

Subcatchment DA-4: Drainage Area #4 Runoff Area=3,343 sf 10.95% Impervious Runoff Depth=0.62"
Flow Length=51' Tc=6.0 min UI Adjusted CN=63 Runoff=0.04 cfs 173 cf

Pond 1P: Gravel Bed Peak Elev=95.82' Storage=166 cf Inflow=0.65 cfs 1,864 cf

Outflow=0.27 cfs 1,874 cf

Peak Elev=97.29' Inflow=0.08 cfs 339 cf

Pond 2P: AD 4 Peak Elev=98.05' Inflow=0.65 cfs 1,864 cf

Primary=0.65 cfs 1,864 cf Secondary=0.00 cfs 0 cf Outflow=0.65 cfs 1,864 cf

Pond MH1: Manhole #1 Peak Elev=96.83' Inflow=0.08 cfs 339 cf 12.0" Round Culvert n=0.013 L=59.5' S=0.0286 '/' Outflow=0.08 cfs 339 cf

12.0" Round Culvert n=0.013 L=23.0' S=0.0200 '/' Outflow=0.08 cfs 339 cf

Link DP-1: Design Point #1 Inflow=0.12 cfs 512 cf
Primary=0.12 cfs 512 cf

Link DP-2: Design Point #2

Inflow=0.02 cfs 102 cf
Primary=0.02 cfs 102 cf

Total Runoff Area = 25,167 sf Runoff Volume = 2,478 cf Average Runoff Depth = 1.18" 68.76% Pervious = 17,306 sf 31.24% Impervious = 7,861 sf

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Summary for Subcatchment DA-1: Drainage Area #1

Runoff = 0.08 cfs @ 12.06 hrs, Volume=

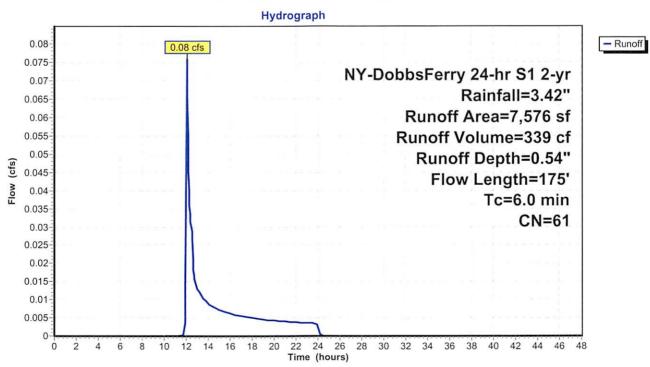
339 cf, Depth= 0.54"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs NY-DobbsFerry 24-hr S1 2-yr Rainfall=3.42"

	Area (sf)	CN	Description		
	d, HSG B				
1.5	7,576		100.00% Pe	rvious Area	
To (min)		Slop (ft/f		Capacity (cfs)	Description
1.7		0.260		V/	Sheet Flow, AB
0.1	. 26	0.115	0 5.09		Grass: Dense n= 0.240 P2= 3.50" Shallow Concentrated Flow, BC Grassed Waterway Kv= 15.0 fps
0.2	51	0.054	0 3.49		Shallow Concentrated Flow, CD Grassed Waterway Kv= 15.0 fps
0.1	. 71	0.057	0 14.08	11.06	
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25' n= 0.010 PVC, smooth interior

2.1 175 Total, Increased to minimum Tc = 6.0 min

Subcatchment DA-1: Drainage Area #1



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Summary for Subcatchment DA-2: Drainage Area #2

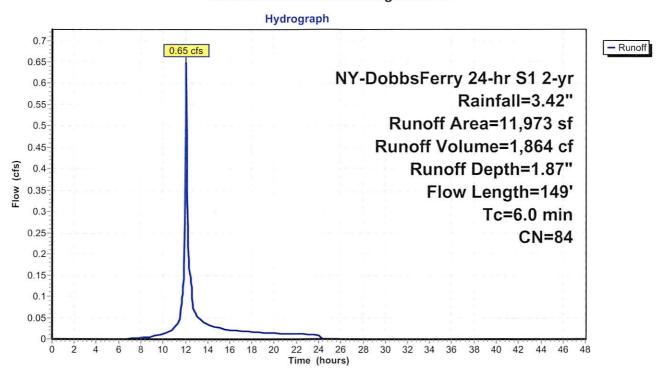
Runoff = 0.65 cfs @ 12.04 hrs, Volume= 1,864 cf, Depth= 1.87"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs NY-DobbsFerry 24-hr S1 2-yr Rainfall=3.42"

Α	rea (sf)	CN E	Description					
	4,478	61 >	75% Grass	cover, Goo	d, HSG B			
	7,495	98 F	aved parki	ng, HSG B				
	11,973	84 V	Veighted A	verage				
	4,478	3	7.40% Perv	ious Area				
	7,495	ϵ	2.60% Imp	ervious Are	ea			
Tc	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
1.8	21	0.1400	0.19		Sheet Flow, AB			
					Grass: Dense n= 0.240 P2= 3.50"			
0.5	128	0.0500	4.54		Shallow Concentrated Flow, BC			
					Paved Kv= 20.3 fps			

2.3 149 Total, Increased to minimum Tc = 6.0 min

Subcatchment DA-2: Drainage Area #2



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Summary for Subcatchment DA-3: Drainage Area #3

Runoff =

0.02 cfs @ 12.06 hrs, Volume=

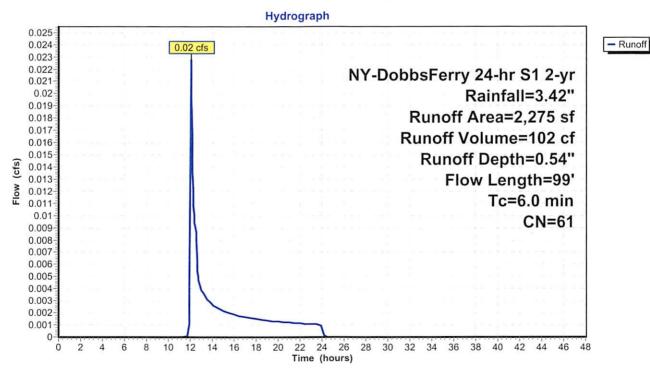
102 cf, Depth= 0.54"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs NY-DobbsFerry 24-hr S1 2-yr Rainfall=3.42"

A	rea (sf)	CN	Description							
	2,275	61	>75% Grass cover, Good, HSG B							
	2,275	9	100.00% Pervious Area							
Tc (min)	Length (feet)	Slope (ft/ft		Capacity (cfs)	Description					
1.9	24	0.1700	0.22	31	Sheet Flow, AB					
0.3	75	0.0670	3.88		Grass: Dense n= 0.240 P2= 3.50" Shallow Concentrated Flow, BC Grassed Waterway Kv= 15.0 fps					

2.2 99 Total, Increased to minimum Tc = 6.0 min

Subcatchment DA-3: Drainage Area #3



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Summary for Subcatchment DA-4: Drainage Area #4

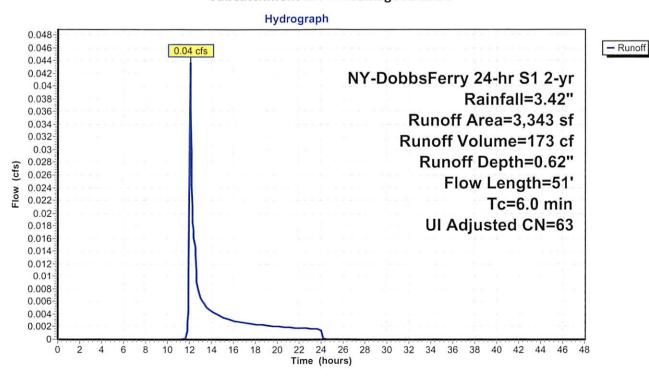
173 cf, Depth= 0.62" Runoff 0.04 cfs @ 12.06 hrs, Volume=

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs NY-DobbsFerry 24-hr S1 2-yr Rainfall=3.42"

_	Α	rea (sf)	CN A	Adj Descr	escription				
		2,977	61	>75%	Grass cove	r, Good, HSG B			
_		366	98	Unco	nnected pa	vement, HSG B			
		3,343	65	63 Weig	nted Avera	ge, UI Adjusted			
		2,977		89.05	% Pervious	Area			
		366		10.95	% Impervio	ous Area			
		366		100.0	0% Unconr	nected			
	Tc	Length	Slope	Velocity	Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	2.2	25	0.1200	0.19		Sheet Flow, AB			
						Grass: Dense n= 0.240 P2= 3.50"			
	0.1	26	0.0650	3.82		Shallow Concentrated Flow, BC			
-	-					Grassed Waterway Kv= 15.0 fps			
				an terrest a reason	140.00				

2.3 51 Total, Increased to minimum Tc = 6.0 min

Subcatchment DA-4: Drainage Area #4



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Appendix C August 2020

NY-DobbsFerry 24-hr S1 2-yr Rainfall=3.42"

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Summary for Pond 1P: Gravel Bed

Inflow Area =

11,973 sf, 62.60% Impervious, Inflow Depth = 1.87" for 2-yr event

Inflow =

0.65 cfs @ 12.04 hrs, Volume=

1,864 cf

Outflow =

0.27 cfs @ 12.00 hrs, Volume=

1,874 cf, Atten= 58%, Lag= 0.0 min

Discarded =

0.27 cfs @ 12.00 hrs, Volume=

1.874 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

Peak Elev= 95.82' @ 12.20 hrs Surf.Area= 740 sf Storage= 166 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow)

Center-of-Mass det. time= 2.3 min (845.6 - 843.3)

Volume	Invert	Avail.Storage	Storage Description	
#1A	95.26'	1,151 cf	18.50'W x 40.00'L x 4.17'H Field A	
			3,083 cf Overall - 204 cf Embedded = 2,878 cf x 40.0% Voids	
#2A	97.26'	154 cf	ADS N-12 15" x 3 Inside #1	
			Inside= 14.8"W x 14.8"H => 1.20 sf x 20.00'L = 24.0 cf	
			Outside= 18.0"W x 18.0"H => 1.60 sf x 20.00'L = 31.9 cf	
			Row Length Adjustment= +13.00' x 1.20 sf x 3 rows	
		. <u></u> .	14.50' Header x 1.20 sf x 2 = 34.8 cf Inside	

1,305 cf Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices			
#1	Discarded	95.26'	16.000 in/hr Exfiltration over Surface area			

Discarded OutFlow Max=0.27 cfs @ 12.00 hrs HW=95.35' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.27 cfs)

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Pond 1P: Gravel Bed - Chamber Wizard Field A

Chamber Model = ADS N-12 15" (ADS N-12® Pipe)

Inside= 14.8"W x 14.8"H => 1.20 sf x 20.00'L = 24.0 cf Outside= 18.0"W x 18.0"H => 1.60 sf x 20.00'L = 31.9 cf Row Length Adjustment= +13.00' x 1.20 sf x 3 rows

18.0" Wide + 60.0" Spacing = 78.0" C-C Row Spacing

1 Chambers/Row x 20.00' Long +13.00' Row Adjustment +1.50' Header x 2 = 36.00' Row Length +24.0" End Stone x 2 = 40.00' Base Length

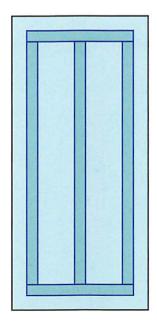
3 Rows x 18.0" Wide + 60.0" Spacing x 2 + 24.0" Side Stone x 2 = 18.50' Base Width 24.0" Base + 18.0" Chamber Height + 8.0" Cover = 4.17' Field Height

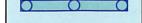
3 Chambers x 24.0 cf +13.00' Row Adjustment x 1.20 sf x 3 Rows + 14.50' Header x 1.20 sf x 2 = 153.6 cf Chamber Storage 3 Chambers x 31.9 cf +13.00' Row Adjustment x 1.60 sf x 3 Rows + 14.50' Header x 1.60 sf x 2 = 204.3 cf Displacement

3,082.5 cf Field - 204.3 cf Chambers = 2,878.2 cf Stone x 40.0% Voids = 1,151.3 cf Stone Storage

Chamber Storage + Stone Storage = 1,304.9 cf = 0.03 af Overall Storage Efficiency = 42.3% Overall System Size = 40.00' x 18.50' x 4.17'

3 Chambers 114.2 cy Field 106.6 cy Stone



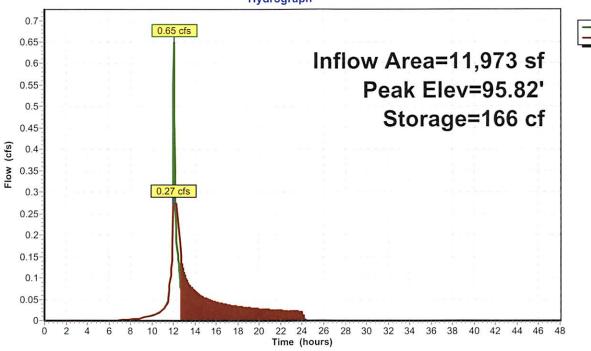


Appendix C August 2020 NY-DobbsFerry 24-hr S1 2-yr Rainfall=3.42" Printed 7/31/2020 1:54:00 PM

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Pond 1P: Gravel Bed







InflowOutflow

Primary

Secondary

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Summary for Pond 2P: AD 4

Inflow Area = 11,973 sf, 62.60% Impervious, Inflow Depth = 1.87" for 2-yr event

Inflow = 0.65 cfs @ 12.04 hrs, Volume= 1,864 cf

Outflow = 0.65 cfs @ 12.04 hrs, Volume= 1,864 cf, Atten= 0%, Lag= 0.0 min

Primary = 0.65 cfs @ 12.04 hrs, Volume= 1,864 cf Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

Peak Elev= 98.05' @ 12.04 hrs

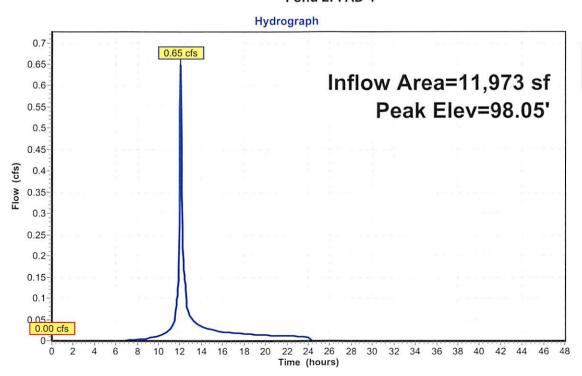
Flood Elev= 101.50'

Device	Routing	Invert	Outlet Devices
#1	Primary	97.48'	10.0" Round Culvert L= 5.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 97.48' / 97.48' S= 0.0000 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.55 sf
#2	Secondary	98.43'	12.0" Round Culvert L= 21.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 98.43' / 98.22' S= 0.0100 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=0.63 cfs @ 12.04 hrs HW=98.04' TW=95.52' (Dynamic Tailwater) 1=Culvert (Barrel Controls 0.63 cfs @ 2.30 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=97.48' TW=97.16' (Dynamic Tailwater) 2=Culvert (Controls 0.00 cfs)

Pond 2P: AD 4



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Summary for Pond MH1: Manhole #1

Inflow Area = 19,549 sf, 38.34% Impervious, Inflow Depth = 0.21" for 2-yr event

Inflow 0.08 cfs @ 12.06 hrs, Volume= 339 cf

339 cf, Atten= 0%, Lag= 0.0 min Outflow 0.08 cfs @ 12.06 hrs, Volume=

339 cf Primary 0.08 cfs @ 12.06 hrs, Volume=

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

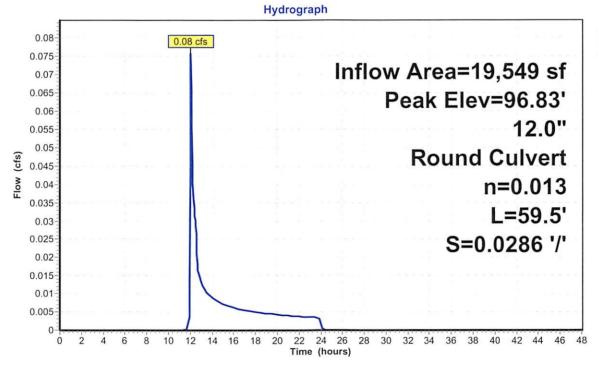
Peak Elev= 96.83' @ 12.06 hrs

Flood Elev= 101.00'

Device	Routing	Invert	Outlet Devices				
#1	Primary	96.70'	12.0" Round Culvert L= 59.5' RCP, square edge headwall, Ke= 0.500				
			Inlet / Outlet Invert= 96.70' / 95.00' S= 0.0286 '/' Cc= 0.900				
			0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf				

Primary OutFlow Max=0.07 cfs @ 12.06 hrs HW=96.83' TW=0.00' (Dynamic Tailwater) **1=Culvert** (Inlet Controls 0.07 cfs @ 1.22 fps)

Pond MH1: Manhole #1





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Summary for Pond MH2: MH2

Inflow Area = 19,549 sf, 38.34% Impervious, Inflow Depth = 0.21" for 2-yr event

Inflow = 0.08 cfs @ 12.06 hrs, Volume= 339 cf

Outflow = 0.08 cfs @ 12.06 hrs, Volume= 339 cf, Atten= 0%, Lag= 0.0 min

Primary = 0.08 cfs @ 12.06 hrs, Volume= 339 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

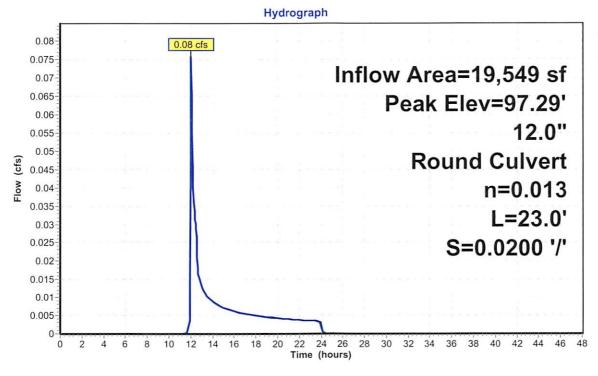
Peak Elev= 97.29' @ 12.06 hrs

Flood Elev= 102.76'

Device	Routing	Invert	Outlet Devices
#1	Primary	97.16'	12.0" Round Culvert L= 23.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 97.16' / 96.70' S= 0.0200 '/' Cc= 0.900
			n= 0.013 Corrugated PF, smooth interior. Flow Area= 0.79 sf

Primary OutFlow Max=0.07 cfs @ 12.06 hrs HW=97.29' TW=96.83' (Dynamic Tailwater) 1=Culvert (Inlet Controls 0.07 cfs @ 1.22 fps)

Pond MH2: MH2





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Summary for Link DP-1: Design Point #1

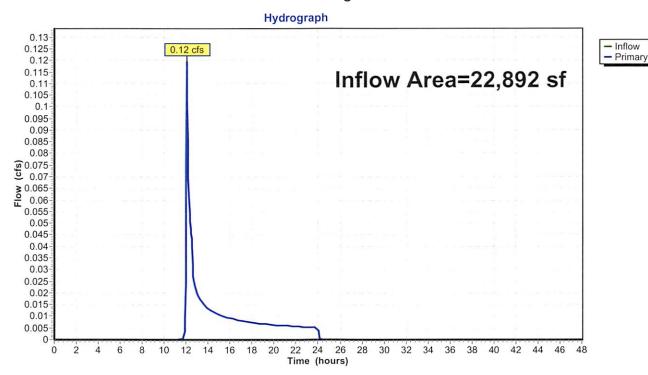
Inflow Area = 22,892 sf, 34.34% Impervious, Inflow Depth = 0.27" for 2-yr event

Inflow 0.12 cfs @ 12.06 hrs, Volume= 512 cf

Primary 0.12 cfs @ 12.06 hrs, Volume= 512 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

Link DP-1: Design Point #1



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Summary for Link DP-2: Design Point #2

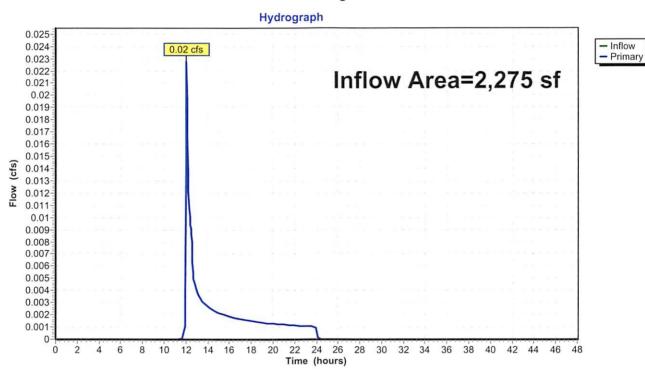
Inflow Area = 2,275 sf, 0.00% Impervious, Inflow Depth = 0.54" for 2-yr event

Inflow = 0.02 cfs @ 12.06 hrs, Volume= 102 cf

Primary = 0.02 cfs @ 12.06 hrs, Volume= 102 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

Link DP-2: Design Point #2



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Appendix C August 2020 NY-DobbsFerry 24-hr S1 10-yr Rainfall=5.06" Printed 7/31/2020 1:54:00 PM Page 15

Time span=0.00-48.00 hrs, dt=0.05 hrs, 961 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment DA-1: Drainage Area #1 Runoff Area=7,576 sf 0.00% Impervious Runoff Depth=1.41"
Flow Length=175' Tc=6.0 min CN=61 Runoff=0.25 cfs 887 cf

Subcatchment DA-2: Drainage Area #2

Runoff Area=11,973 sf 62.60% Impervious Runoff Depth=3.33"

Flow Length=149' Tc=6.0 min CN=84 Runoff=1.05 cfs 3,318 cf

Subcatchment DA-3: Drainage Area #3

Runoff Area=2,275 sf 0.00% Impervious Runoff Depth=1.41"

Flow Length=99' Tc=6.0 min CN=61 Runoff=0.08 cfs 266 cf

Subcatchment DA-4: Drainage Area #4 Runoff Area=3,343 sf 10.95% Impervious Runoff Depth=1.55"
Flow Length=51' Tc=6.0 min UI Adjusted CN=63 Runoff=0.13 cfs 431 cf

Pond 1P: Gravel Bed

Peak Elev=96.97' Storage=507 cf Inflow=1.05 cfs 3,318 cf

Outflow=0.27 cfs 3,334 cf

Pond 2P: AD 4 Peak Elev=98.23' Inflow=1.05 cfs 3,318 cf
Primary=1.05 cfs 3,318 cf Secondary=0.00 cfs 0 cf Outflow=1.05 cfs 3,318 cf

Pond MH1: Manhole #1 Peak Elev=96.94' Inflow=0.25 cfs 887 cf 12.0" Round Culvert n=0.013 L=59.5' S=0.0286 '/' Outflow=0.25 cfs 887 cf

Pond MH2: MH2 Peak Elev=97.40' Inflow=0.25 cfs 887 cf 12.0" Round Culvert n=0.013 L=23.0' S=0.0200'/' Outflow=0.25 cfs 887 cf

Link DP-1: Design Point #1 Inflow=0.38 cfs 1,318 cf
Primary=0.38 cfs 1,318 cf

Link DP-2: Design Point #2

Inflow=0.08 cfs 266 cf
Primary=0.08 cfs 266 cf

Total Runoff Area = 25,167 sf Runoff Volume = 4,902 cf Average Runoff Depth = 2.34" 68.76% Pervious = 17,306 sf 31.24% Impervious = 7,861 sf

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Summary for Subcatchment DA-1: Drainage Area #1

Runoff = 0.25 cfs @ 12.05 hrs, Volume=

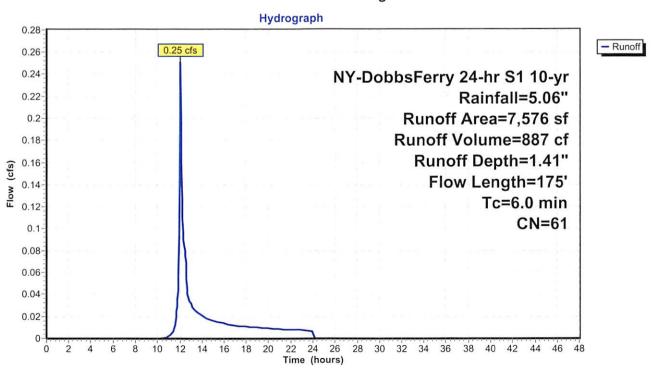
887 cf, Depth= 1.41"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs NY-DobbsFerry 24-hr S1 10-yr Rainfall=5.06"

A	rea (sf)	CN I	Description							
	7,576	61	>75% Grass cover, Good, HSG B							
	7,576		.00.00% Pei	vious Area						
Tc (min)	Length (feet)	Slope (ft/ft		Capacity (cfs)	Description					
1.7	27	0.2600	0.26	,,,,,	Sheet Flow, AB					
0.1	26	0.1150	5.09		Grass: Dense n= 0.240 P2= 3.50" Shallow Concentrated Flow, BC					
0.1	20	0.1150	3.03		Grassed Waterway Kv= 15.0 fps					
0.2	51	0.0540	3.49		Shallow Concentrated Flow, CD					
					Grassed Waterway Kv= 15.0 fps					
0.1	71	0.0570	14.08	11.06	Pipe Channel, DE					
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'					
					n= 0.010 PVC, smooth interior					

2.1 175 Total, Increased to minimum Tc = 6.0 min

Subcatchment DA-1: Drainage Area #1



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Summary for Subcatchment DA-2: Drainage Area #2

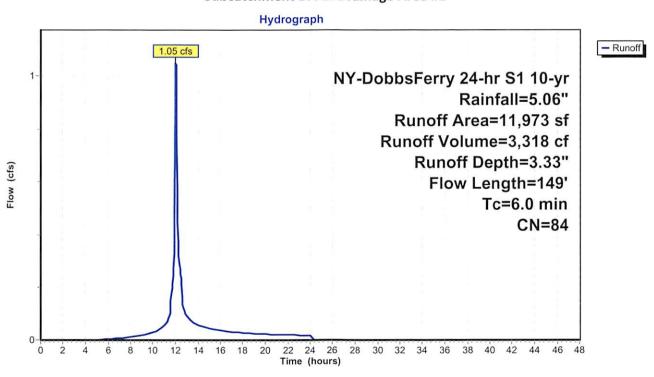
Runoff = 1.05 cfs @ 12.04 hrs, Volume= 3,318 cf, Depth= 3.33"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs NY-DobbsFerry 24-hr S1 10-yr Rainfall=5.06"

Ar	rea (sf)	CN [N Description							
	4,478	61 >	>75% Grass cover, Good, HSG B							
	7,495	98 F	aved parki	ng, HSG B						
,	11,973	84 \	Veighted A	verage						
	4,478	3	7.40% Perv	ious Area						
	7,495	6	2.60% Imp	ervious Are	ea					
Tc	Length	Slope	Velocity	Capacity	Description					
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
1.8	21	0.1400	0.19		Sheet Flow, AB					
					Grass: Dense n= 0.240 P2= 3.50"					
0.5	128	0.0500	4.54		Shallow Concentrated Flow, BC					
_					Paved Kv= 20.3 fps					

2.3 149 Total, Increased to minimum Tc = 6.0 min

Subcatchment DA-2: Drainage Area #2



Summary for Subcatchment DA-3: Drainage Area #3

Runoff 0.08 cfs @ 12.05 hrs, Volume=

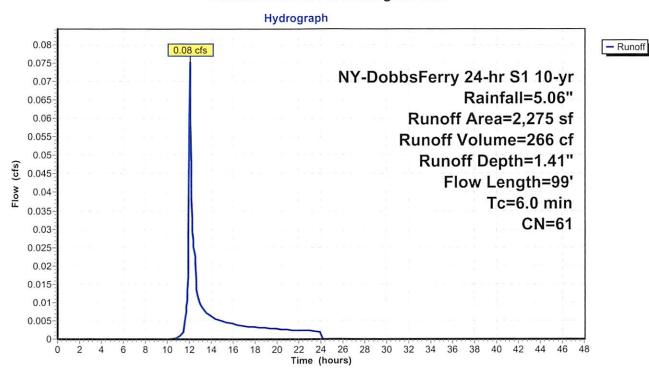
266 cf, Depth= 1.41"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs NY-DobbsFerry 24-hr S1 10-yr Rainfall=5.06"

A	rea (sf)	CN [CN Description							
	2,275	61 >	1 >75% Grass cover, Good, HSG B							
19-	2,275	1	100.00% Pervious Area							
Tc	Length	Slope	Velocity	Capacity	Description					
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
1.9	24	0.1700	0.22		Sheet Flow, AB					
					Grass: Dense n= 0.240 P2= 3.50"					
0.3	75	0.0670	3.88		Shallow Concentrated Flow, BC					
				<i></i>	Grassed Waterway Kv= 15.0 fps					
2.2	00	T			T 60 :					

2.2 Total, Increased to minimum Tc = 6.0 min

Subcatchment DA-3: Drainage Area #3



Summary for Subcatchment DA-4: Drainage Area #4

Runoff = 0.13 cfs @ 12.05 hrs, Volume=

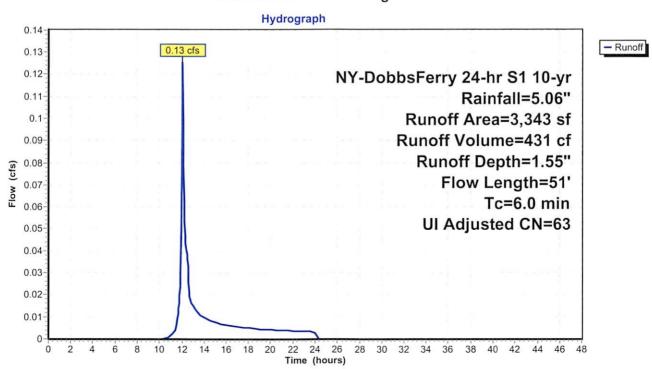
431 cf, Depth= 1.55"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs NY-DobbsFerry 24-hr S1 10-yr Rainfall=5.06"

	Α	rea (sf)	CN A	dj Descr	iption	
		2,977	61	>75%	Grass cove	er, Good, HSG B
		366	98	Uncor	nnected pa	vement, HSG B
		3,343	65	63 Weigh	nted Avera	ge, UI Adjusted
		2,977		89.05	% Pervious	Area
		366		10.95	% Impervio	ous Area
		366		100.0	0% Unconr	nected
	Tc	Length	Slope	Velocity	Capacity	Description
-	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	2.2	25	0.1200	0.19		Sheet Flow, AB
						Grass: Dense n= 0.240 P2= 3.50"
	0.1	26	0.0650	3.82		Shallow Concentrated Flow, BC
						Grassed Waterway Kv= 15.0 fps

2.3 51 Total, Increased to minimum Tc = 6.0 min

Subcatchment DA-4: Drainage Area #4



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Appendix C August 2020
NY-DobbsFerry 24-hr S1 10-yr Rainfall=5.06"
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Summary for Pond 1P: Gravel Bed

inflow Area =

11,973 sf, 62.60% Impervious, Inflow Depth = 3.33" for 10-yr event

Inflow =

1.05 cfs @ 12.04 hrs, Volume=

3,318 cf

Outflow =

0.27 cfs @ 11.95 hrs, Volume=

3,334 cf, Atten= 74%, Lag= 0.0 min

Discarded =

0.27 cfs @ 11.95 hrs, Volume=

3,334 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

Peak Elev= 96.97' @ 12.39 hrs Surf.Area= 740 sf Storage= 507 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow)

Center-of-Mass det. time= 8.6 min (832.9 - 824.3)

Volume	Invert	Avail.Storage	Storage Description	
#1A	95.26'	1,151 cf	18.50'W x 40.00'L x 4.17'H Field A	
			3,083 cf Overall - 204 cf Embedded = 2,878 cf x 40.0% Voids	
#2A	97.26'	154 cf	ADS N-12 15" x 3 Inside #1	
			Inside= 14.8"W x 14.8"H => 1.20 sf x 20.00'L = 24.0 cf	
			Outside= 18.0"W x 18.0"H => 1.60 sf x 20.00'L = 31.9 cf	
			Row Length Adjustment= +13.00' x 1.20 sf x 3 rows	
			14.50' Header x 1.20 sf x 2 = 34.8 cf Inside	

1,305 cf Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices			
#1	Discarded	95.26'	16.000 in/hr Exfiltration over Surface area			

Discarded OutFlow Max=0.27 cfs @ 11.95 hrs HW=95.36' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.27 cfs)

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Pond 1P: Gravel Bed - Chamber Wizard Field A

Chamber Model = ADS N-12 15" (ADS N-12® Pipe)

Inside= 14.8"W x 14.8"H => 1.20 sf x 20.00'L = 24.0 cf Outside= 18.0"W x 18.0"H => 1.60 sf x 20.00'L = 31.9 cf Row Length Adjustment= +13.00' x 1.20 sf x 3 rows

18.0" Wide + 60.0" Spacing = 78.0" C-C Row Spacing

1 Chambers/Row x 20.00' Long +13.00' Row Adjustment +1.50' Header x 2 = 36.00' Row Length +24.0" End Stone x 2 = 40.00' Base Length

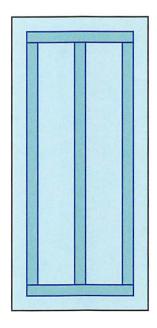
3 Rows x 18.0" Wide + 60.0" Spacing x 2 + 24.0" Side Stone x 2 = 18.50' Base Width 24.0" Base + 18.0" Chamber Height + 8.0" Cover = 4.17' Field Height

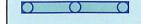
3 Chambers x 24.0 cf +13.00' Row Adjustment x 1.20 sf x 3 Rows + 14.50' Header x 1.20 sf x 2 = 153.6 cf Chamber Storage 3 Chambers x 31.9 cf +13.00' Row Adjustment x 1.60 sf x 3 Rows + 14.50' Header x 1.60 sf x 2 = 204.3 cf Displacement

3,082.5 cf Field - 204.3 cf Chambers = 2,878.2 cf Stone x 40.0% Voids = 1,151.3 cf Stone Storage

Chamber Storage + Stone Storage = 1,304.9 cf = 0.03 af Overall Storage Efficiency = 42.3% Overall System Size = 40.00' x 18.50' x 4.17'

3 Chambers 114.2 cy Field 106.6 cy Stone





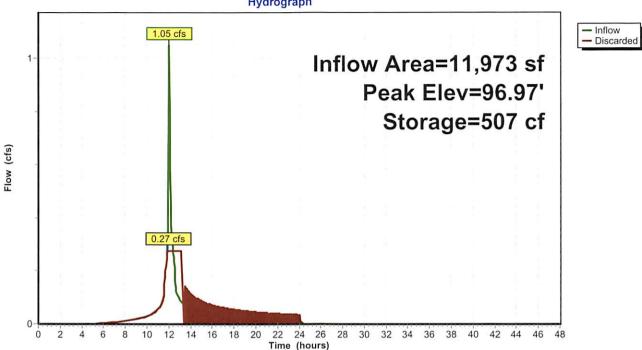
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Pond 1P: Gravel Bed





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Summary for Pond 2P: AD 4

Inflow Area = 11,973 sf, 62.60% Impervious, Inflow Depth = 3.33" for 10-yr event

Inflow = 1.05 cfs @ 12.04 hrs, Volume= 3,318 cf

Outflow = 1.05 cfs @ 12.04 hrs, Volume= 3,318 cf, Atten= 0%, Lag= 0.0 min

Primary = 1.05 cfs @ 12.04 hrs, Volume= 3,318 cf Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

Peak Elev= 98.23' @ 12.04 hrs

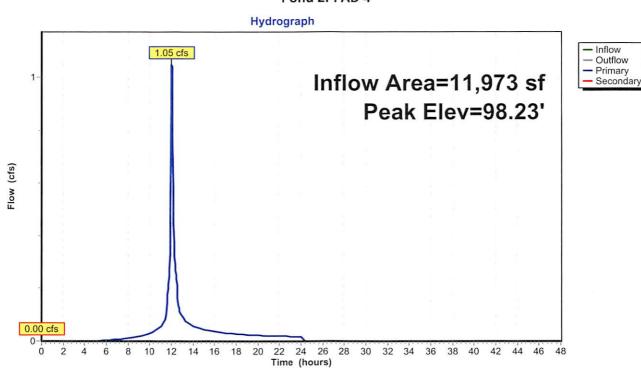
Flood Elev= 101.50'

Device	Routing	Invert	Outlet Devices
#1	Primary	97.48'	10.0" Round Culvert L= 5.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 97.48' / 97.48' S= 0.0000 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.55 sf
#2	Secondary	98.43'	12.0" Round Culvert L= 21.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 98.43' / 98.22' S= 0.0100 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=1.02 cfs @ 12.04 hrs HW=98.21' TW=95.98' (Dynamic Tailwater) 1=Culvert (Barrel Controls 1.02 cfs @ 2.66 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=97.48' TW=97.16' (Dynamic Tailwater) 2=Culvert (Controls 0.00 cfs)

Pond 2P: AD 4



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Summary for Pond MH1: Manhole #1

Inflow Area = 19,549 sf, 38.34% Impervious, Inflow Depth = 0.54" for 10-yr event

Inflow = 0.25 cfs @ 12.05 hrs, Volume= 887 cf

Outflow = 0.25 cfs @ 12.05 hrs, Volume= 887 cf, Atten= 0%, Lag= 0.0 min

Primary = 0.25 cfs @ 12.05 hrs, Volume= 887 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

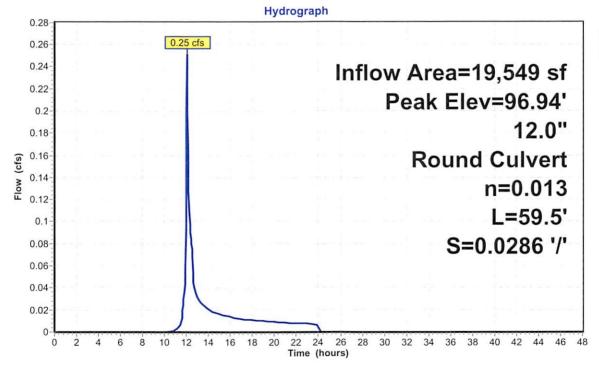
Peak Elev= 96.94' @ 12.05 hrs

Flood Elev= 101.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	96.70'	12.0" Round Culvert L= 59.5' RCP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 96.70' / 95.00' S= 0.0286 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior. Flow Area= 0.79 sf

Primary OutFlow Max=0.25 cfs @ 12.05 hrs HW=96.94' TW=0.00' (Dynamic Tailwater) 1=Culvert (Inlet Controls 0.25 cfs @ 1.68 fps)

Pond MH1: Manhole #1





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Summary for Pond MH2: MH2

Inflow Area = 19,549 sf, 38.34% Impervious, Inflow Depth = 0.54" for 10-yr event

Inflow = 0.25 cfs @ 12.05 hrs, Volume= 887 cf

Outflow = 0.25 cfs @ 12.05 hrs, Volume= 887 cf, Atten= 0%, Lag= 0.0 min

Primary = 0.25 cfs @ 12.05 hrs, Volume= 887 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

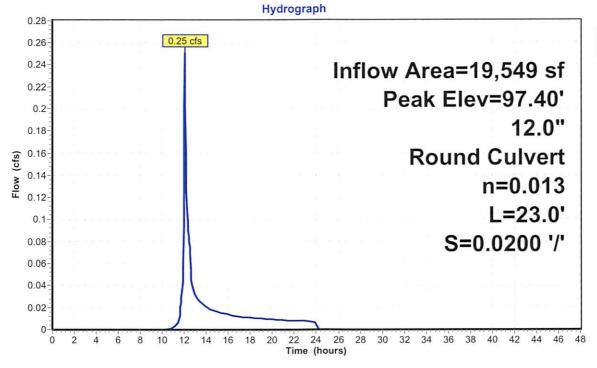
Peak Elev= 97.40' @ 12.05 hrs

Flood Elev= 102.76'

Device	Routing	Invert	Outlet Devices
#1	Primary	97.16'	12.0" Round Culvert L= 23.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 97.16' / 96.70' S= 0.0200 '/' Cc= 0.900
			n= 0.013 Corrugated PF, smooth interior. Flow Area= 0.79 sf

Primary OutFlow Max=0.25 cfs @ 12.05 hrs HW=97.40' TW=96.94' (Dynamic Tailwater) 1=Culvert (Inlet Controls 0.25 cfs @ 1.68 fps)

Pond MH2: MH2





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Summary for Link DP-1: Design Point #1

Inflow Area =

22,892 sf, 34.34% Impervious, Inflow Depth = 0.69" for 10-yr event

Inflow

0.38 cfs @ 12.05 hrs, Volume=

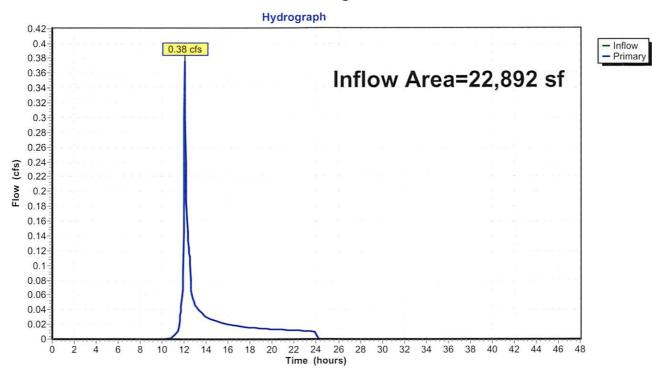
1,318 cf

0.38 cfs @ 12.05 hrs, Volume= Primary

1,318 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

Link DP-1: Design Point #1



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Summary for Link DP-2: Design Point #2

Inflow Area =

2,275 sf, 0.00% Impervious, Inflow Depth = 1.41" for 10-yr event

Inflow =

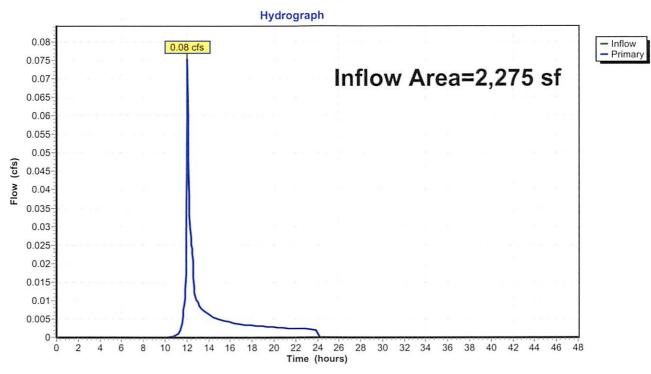
Primary

0.08 cfs @ 12.05 hrs, Volume= 0.08 cfs @ 12.05 hrs, Volume= 266 cf

266 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

Link DP-2: Design Point #2



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Appendix C August 2020

NY-DobbsFerry 24-hr S1 100-yr Rainfall=8.90"

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Time span=0.00-48.00 hrs, dt=0.05 hrs, 961 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment DA-1: Drainage Area #1 Runoff Area=7,576 sf 0.00% Impervious Runoff Depth=4.14" Flow Length=175' Tc=6.0 min CN=61 Runoff=0.75 cfs 2,617 cf

Subcatchment DA-2: Drainage Area #2

Runoff Area=11,973 sf 62.60% Impervious Runoff Depth=6.96"

Flow Length=149' Tc=6.0 min CN=84 Runoff=1.95 cfs 6,947 cf

Subcatchment DA-3: Drainage Area #3

Runoff Area=2,275 sf 0.00% Impervious Runoff Depth=4.14"

Flow Length=99' Tc=6.0 min CN=61 Runoff=0.22 cfs 786 cf

Subcatchment DA-4: Drainage Area #4 Runoff Area=3,343 sf 10.95% Impervious Runoff Depth=4.39"
Flow Length=51' Tc=6.0 min UI Adjusted CN=63 Runoff=0.35 cfs 1,223 cf

Pond 1P: Gravel Bed

Peak Elev=99.22' Storage=1,245 cf Inflow=1.83 cfs 6,171 cf

Outflow=0.27 cfs 6,186 cf

12.0" Round Culvert n=0.013 L=23.0' S=0.0200'/' Outflow=1.25 cfs 3,392 cf

Pond 2P: AD 4 Peak Elev=98.97' Inflow=1.95 cfs 6,947 cf

Primary=1.83 cfs 6,171 cf Secondary=0.91 cfs 776 cf Outflow=1.95 cfs 6,947 cf

Pond MH1: Manhole #1 Peak Elev=97.29' Inflow=1.25 cfs 3,392 cf 12.0" Round Culvert n=0.013 L=59.5' S=0.0286'/' Outflow=1.25 cfs 3,392 cf

Pond MH2: MH2 Peak Elev=97.75' Inflow=1.25 cfs 3,392 cf

Link DP-1: Design Point #1 Inflow=1.41 cfs 4,615 cf
Primary=1.41 cfs 4,615 cf

Link DP-2: Design Point #2 Inflow=0.22 cfs 786 cf
Primary=0.22 cfs 786 cf

Total Runoff Area = 25,167 sf Runoff Volume = 11,572 cf Average Runoff Depth = 5.52"
68.76% Pervious = 17,306 sf 31.24% Impervious = 7,861 sf

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Summary for Subcatchment DA-1: Drainage Area #1

Runoff = 0.75 cfs @ 12.05 hrs, Volume=

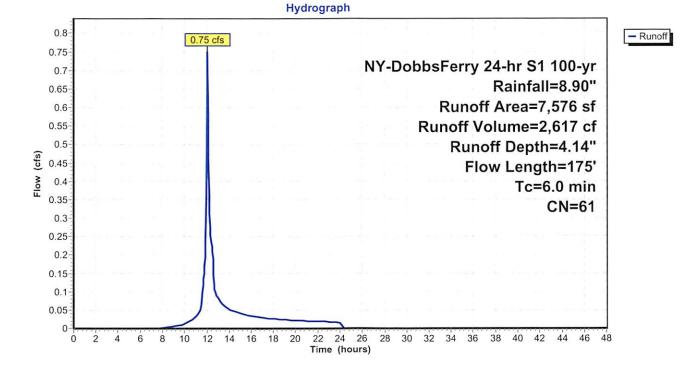
2,617 cf, Depth= 4.14"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs NY-DobbsFerry 24-hr S1 100-yr Rainfall=8.90"

A	rea (sf)	CN D	escription		
	7,576	61 >	75% Grass	cover, Goo	d, HSG B
	7,576	1	00.00% Per	vious Area	
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.7	27	0.2600	0.26		Sheet Flow, AB
					Grass: Dense n= 0.240 P2= 3.50"
0.1	26	0.1150	5.09		Shallow Concentrated Flow, BC
	201	0.12001010	2.02		Grassed Waterway Kv= 15.0 fps
0.2	51	0.0540	3.49		Shallow Concentrated Flow, CD
	_				Grassed Waterway Kv= 15.0 fps
0.1	71	0.0570	14.08	11.06	Pipe Channel, DE
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'
1					n= 0.010 PVC, smooth interior

2.1 175 Total, Increased to minimum Tc = 6.0 min

Subcatchment DA-1: Drainage Area #1



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Summary for Subcatchment DA-2: Drainage Area #2

Runoff = 1.95 cfs @ 12.04 hrs, Volume=

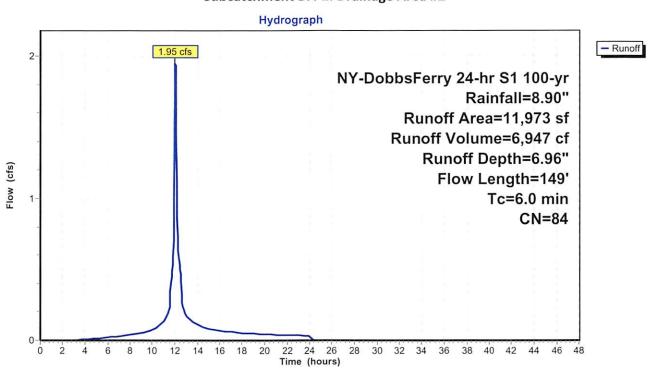
6,947 cf, Depth= 6.96"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs NY-DobbsFerry 24-hr S1 100-yr Rainfall=8.90"

	Α	rea (sf)	CN	N Description							
		4,478	61	51 >75% Grass cover, Good, HSG B							
		7,495	98	Paved parki	ng, HSG B						
		11,973	84	Weighted A	verage						
		4,478		37.40% Per	ious Area						
		7,495		52.60% Imp	ervious Are	ea					
	Tc	Length	Slop	e Velocity	Capacity	Description					
	(min)	(feet)	(ft/ft) (ft/sec)	(cfs)						
	1.8	21	0.140	0.19		Sheet Flow, AB					
						Grass: Dense n= 0.240 P2= 3.50"					
	0.5	128	0.050	4.54		Shallow Concentrated Flow, BC					
_						Paved Kv= 20.3 fps					

2.3 149 Total, Increased to minimum Tc = 6.0 min

Subcatchment DA-2: Drainage Area #2



Summary for Subcatchment DA-3: Drainage Area #3

Runoff =

0.22 cfs @ 12.05 hrs, Volume=

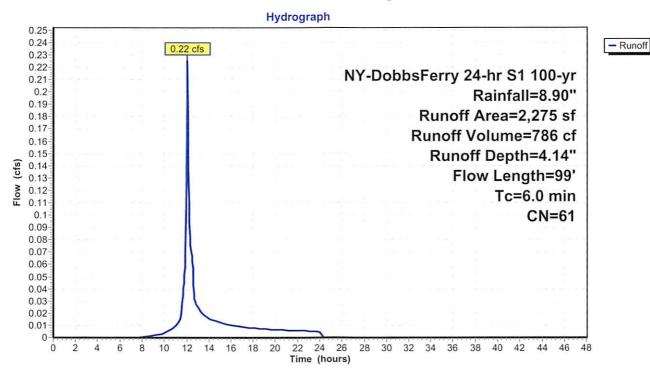
786 cf, Depth= 4.14"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs NY-DobbsFerry 24-hr S1 100-yr Rainfall=8.90"

0	А	rea (sf)	CN Description						
2,275 61 >75% Grass cover, Good, HSG B						od, HSG B			
		2,275	5 100.00% Pervious Area						
	Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description			
	1.9	24	0.1700	0.22		Sheet Flow, AB			
	0.3	75	0.0670	3.88		Grass: Dense n= 0.240 P2= 3.50" Shallow Concentrated Flow, BC Grassed Waterway Kv= 15.0 fps			

2.2 99 Total, Increased to minimum Tc = 6.0 min

Subcatchment DA-3: Drainage Area #3



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Summary for Subcatchment DA-4: Drainage Area #4

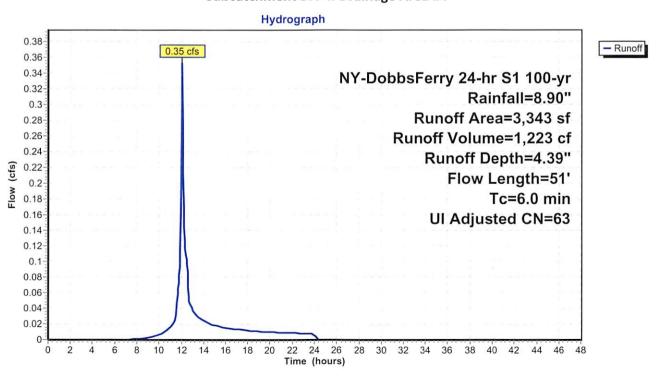
Runoff 0.35 cfs @ 12.04 hrs, Volume= 1,223 cf, Depth= 4.39"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs NY-DobbsFerry 24-hr S1 100-yr Rainfall=8.90"

A	rea (sf)	CN A	Adj Descr	iption		
	2,977	61	>75%	Grass cove	r, Good, HSG B	
	366	98	Unco	nnected pa	vement, HSG B	
	3,343	65	63 Weig	nted Avera	ge, UI Adjusted	
	2,977		89.05	% Pervious	Area	
	366		10.95	% Impervio	ous Area	
	366		100.0	00.00% Unconnected		
Tc	Length	Slope	Velocity	Capacity	Description	
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
2.2	25	0.1200	0.19		Sheet Flow, AB	
					Grass: Dense n= 0.240 P2= 3.50"	
0.1	26	0.0650	3.82		Shallow Concentrated Flow, BC	
					Grassed Waterway Kv= 15.0 fps	
2.3	51	Total,	Increased t	o minimun	n Tc = 6.0 min	

51 Total, Increased to minimum Tc = 6.0 min

Subcatchment DA-4: Drainage Area #4



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Appendix C August 2020 NY-DobbsFerry 24-hr S1 100-yr Rainfall=8.90" Printed 7/31/2020 1:54:01 PM Page 33

Summary for Pond 1P: Gravel Bed

Inflow Area =

11,973 sf, 62.60% Impervious, Inflow Depth = 6.18" for 100-yr event

Inflow

1.83 cfs @ 12.04 hrs, Volume=

6,171 cf

Outflow =

0.27 cfs @ 11.65 hrs, Volume=

6,186 cf, Atten= 85%, Lag= 0.0 min

Discarded =

0.27 cfs @ 11.65 hrs, Volume=

6,186 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 99.22' @ 12.19 hrs Surf.Area= 740 sf Storage= 1,245 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow)

Center-of-Mass det. time= 19.7 min (827.0 - 807.2)

Volume	Invert	Avail.Storage	Storage Description	
#1A	95.26'	1,151 cf	18.50'W x 40.00'L x 4.17'H Field A	
			3,083 cf Overall - 204 cf Embedded = 2,878 cf x 40.0% Voids	
#2A	97.26'	154 cf	ADS N-12 15" x 3 Inside #1	
			Inside= 14.8"W x 14.8"H => 1.20 sf x 20.00'L = 24.0 cf	
			Outside= 18.0"W x 18.0"H => 1.60 sf x 20.00'L = 31.9 cf	
			Row Length Adjustment= +13.00' x 1.20 sf x 3 rows	
			14.50' Header x 1.20 sf x 2 = 34.8 cf Inside	

1,305 cf Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	95.26'	16.000 in/hr Exfiltration over Surface area

Discarded OutFlow Max=0.27 cfs @ 11.65 hrs HW=95.34' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.27 cfs)

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Pond 1P: Gravel Bed - Chamber Wizard Field A

Chamber Model = ADS N-12 15" (ADS N-12® Pipe)

Inside= 14.8"W x 14.8"H => 1.20 sf x 20.00'L = 24.0 cf Outside= 18.0"W x 18.0"H => 1.60 sf x 20.00'L = 31.9 cf Row Length Adjustment= +13.00' x 1.20 sf x 3 rows

18.0" Wide + 60.0" Spacing = 78.0" C-C Row Spacing

1 Chambers/Row x 20.00' Long +13.00' Row Adjustment +1.50' Header x 2 = 36.00' Row Length +24.0" End Stone x 2 = 40.00' Base Length

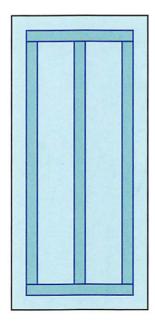
3 Rows x 18.0" Wide + 60.0" Spacing x 2 + 24.0" Side Stone x 2 = 18.50' Base Width 24.0" Base + 18.0" Chamber Height + 8.0" Cover = 4.17' Field Height

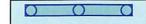
3 Chambers x 24.0 cf +13.00' Row Adjustment x 1.20 sf x 3 Rows + 14.50' Header x 1.20 sf x 2 = 153.6 cf Chamber Storage 3 Chambers x 31.9 cf +13.00' Row Adjustment x 1.60 sf x 3 Rows + 14.50' Header x 1.60 sf x 2 = 204.3 cf Displacement

3,082.5 cf Field - 204.3 cf Chambers = 2,878.2 cf Stone x 40.0% Voids = 1,151.3 cf Stone Storage

Chamber Storage + Stone Storage = 1,304.9 cf = 0.03 afOverall Storage Efficiency = 42.3%Overall System Size = $40.00' \times 18.50' \times 4.17'$

3 Chambers 114.2 cy Field 106.6 cy Stone

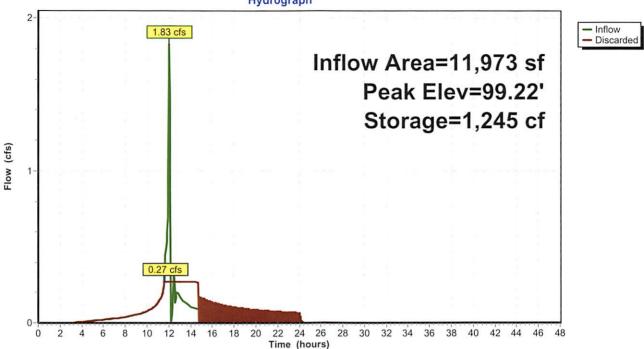




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Pond 1P: Gravel Bed





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Summary for Pond 2P: AD 4

Inflow Area = 11,973 sf, 62.60% Impervious, Inflow Depth = 6.96" for 100-yr event Inflow 1.95 cfs @ 12.04 hrs, Volume= 6,947 cf 1.95 cfs @ 12.04 hrs, Volume= 6,947 cf, Atten= 0%, Lag= 0.0 min Outflow Primary 1.83 cfs @ 12.04 hrs, Volume= 6,171 cf 776 cf Secondary = 0.91 cfs @ 12.22 hrs, Volume=

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 98.97' @ 12.22 hrs

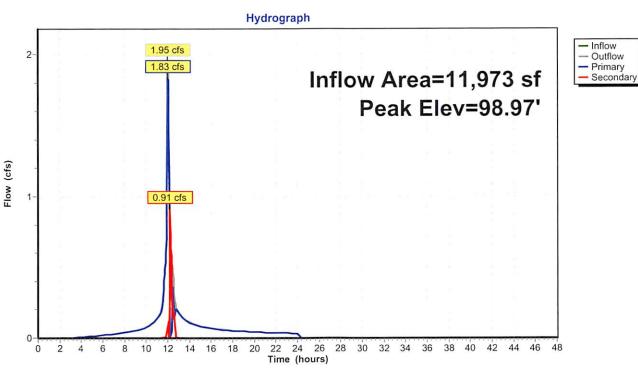
Flood Elev= 101.50'

Device	Routing	Invert	Outlet Devices
#1	Primary	97.48'	10.0" Round Culvert L= 5.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 97.48' / 97.48' S= 0.0000 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.55 sf
#2	Secondary	98.43'	12.0" Round Culvert L= 21.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 98.43' / 98.22' S= 0.0100 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=1.77 cfs @ 12.04 hrs HW=98.59' TW=97.71' (Dynamic Tailwater) 1=Culvert (Barrel Controls 1.77 cfs @ 3.25 fps)

Secondary OutFlow Max=0.82 cfs @ 12.22 hrs HW=98.93' TW=97.73' (Dynamic Tailwater) **1**_2=Culvert (Barrel Controls 0.82 cfs @ 3.03 fps)

Pond 2P: AD 4



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Summary for Pond MH1: Manhole #1

Inflow Area = 19,549 sf, 38.34% Impervious, Inflow Depth = 2.08" for 100-yr event

Inflow 1.25 cfs @ 12.21 hrs, Volume= 3,392 cf

Outflow = 1.25 cfs @ 12.21 hrs, Volume= 3,392 cf, Atten= 0%, Lag= 0.0 min

1.25 cfs @ 12.21 hrs, Volume= 3,392 cf Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

Peak Elev= 97.29' @ 12.21 hrs

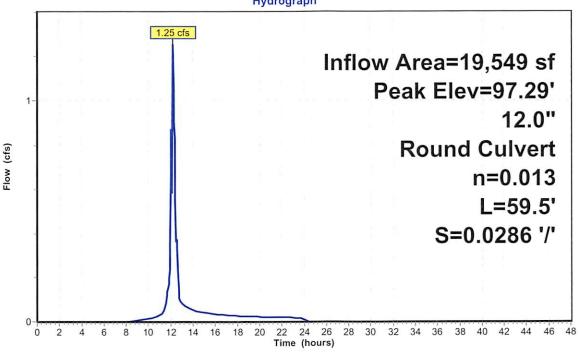
Flood Elev= 101.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	96.70'	12.0" Round Culvert L= 59.5' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 96.70' / 95.00' S= 0.0286 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=1.18 cfs @ 12.21 hrs HW=97.27' TW=0.00' (Dynamic Tailwater) 1=Culvert (Inlet Controls 1.18 cfs @ 2.57 fps)

Pond MH1: Manhole #1

Hydrograph





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Summary for Pond MH2: MH2

Inflow Area = 19,549 sf, 38.34% Impervious, Inflow Depth = 2.08" for 100-yr event

Inflow 1.25 cfs @ 12.21 hrs, Volume= 3,392 cf

Outflow 1.25 cfs @ 12.21 hrs, Volume= 3,392 cf, Atten= 0%, Lag= 0.0 min

Primary 1.25 cfs @ 12.21 hrs, Volume= 3,392 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

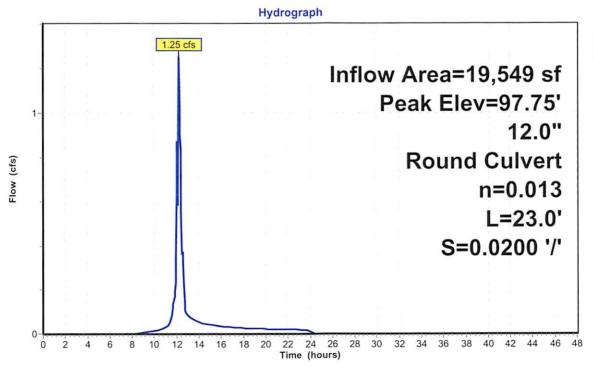
Peak Elev= 97.75' @ 12.22 hrs

Flood Elev= 102.76'

Device	Routing	Invert	Outlet Devices
#1	Primary	97.16'	12.0" Round Culvert L= 23.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 97.16' / 96.70' S= 0.0200 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=1.16 cfs @ 12.21 hrs HW=97.73' TW=97.27' (Dynamic Tailwater) 1=Culvert (Outlet Controls 1.16 cfs @ 3.59 fps)

Pond MH2: MH2





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Summary for Link DP-1: Design Point #1

Inflow Area =

22,892 sf, 34.34% Impervious, Inflow Depth = 2.42" for 100-yr event

Inflow =

1.41 cfs @ 12.21 hrs, Volume=

4,615 cf

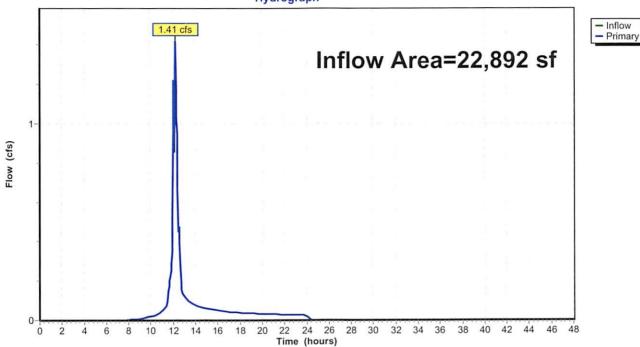
Primary = 1.41 cfs @ 12.21 hrs, Volume=

4,615 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

Link DP-1: Design Point #1

Hydrograph



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Summary for Link DP-2: Design Point #2

Inflow Area =

2,275 sf, 0.00% Impervious, Inflow Depth = 4.14" for 100-yr event

Inflow

0.22 cfs @ 12.05 hrs, Volume=

786 cf

Primary 0.22 cfs @ 12.05 hrs, Volume=

786 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

Link DP-2: Design Point #2

